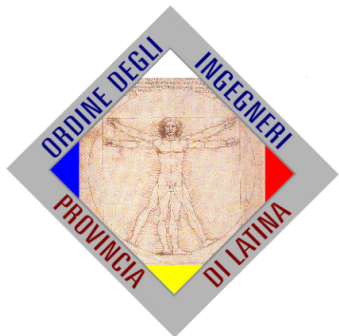




ORDINE DEGLI INGEGNERI DELLA PROVINCIA DI LATINA

con il contributo incondizionato di

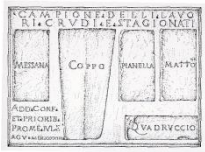


Seminario webinar "RINFORZO E CONSOLIDAMENTO STATICO E ANTISISMICO DEGLI EDIFICI ESISTENTI"

Principi di meccanica delle murature e di archi e volte per la valutazione del comportamento statico e della risposta sismica degli edifici storici in riferimento al quadro normativo.

Analisi del danno e delle lesioni sugli edifici storici, casistiche e approccio alla lettura del quadro fessurativo

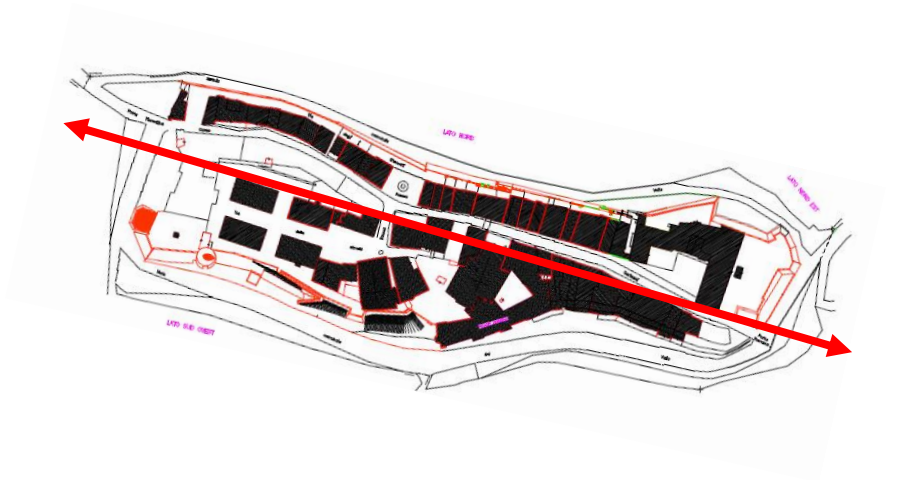
Ing. Giovanni Cangi – libero professionista



Terremoto di Citerna-Monterchi (26 aprile 1917)



Monterchi (AR)

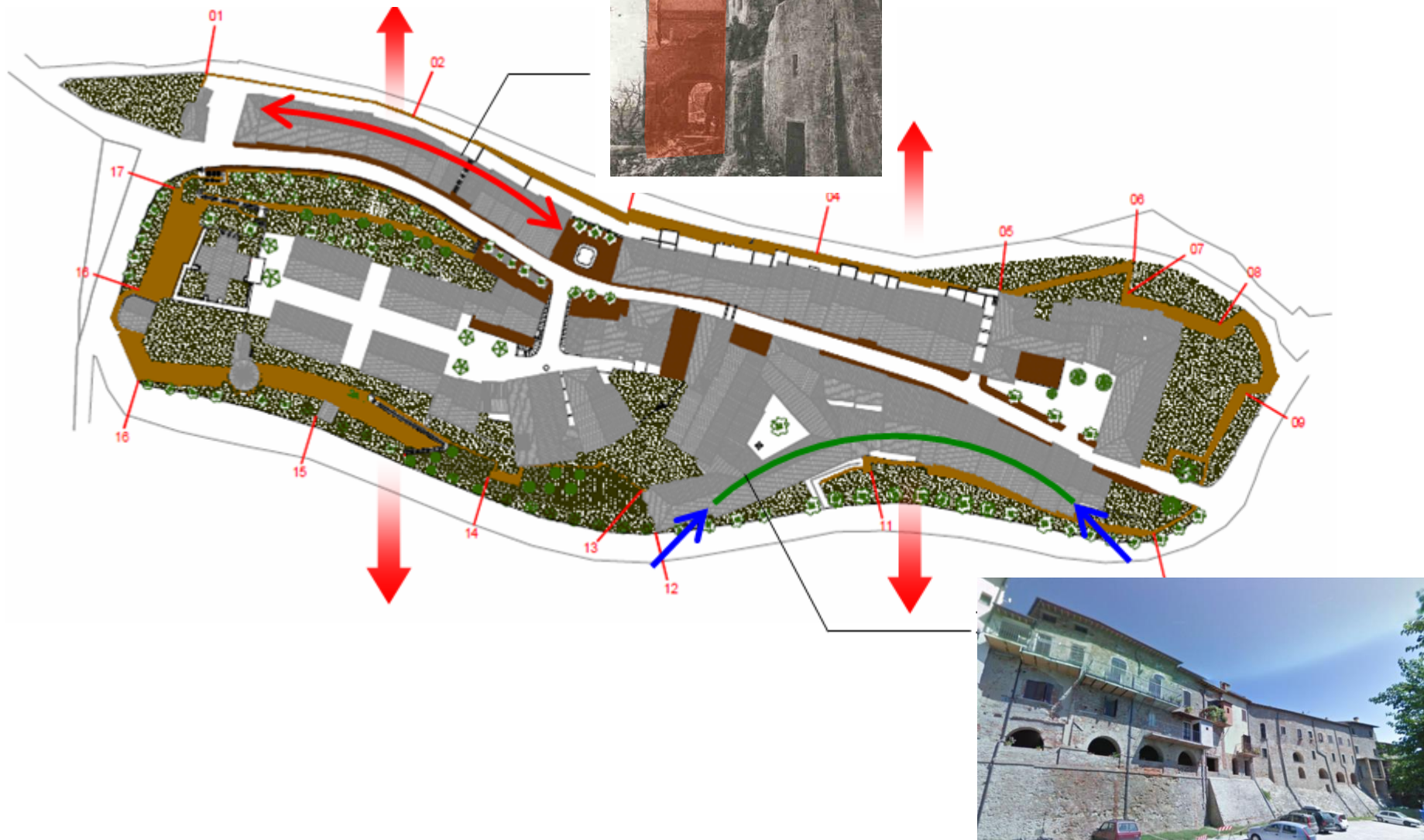


Citerna (PG)

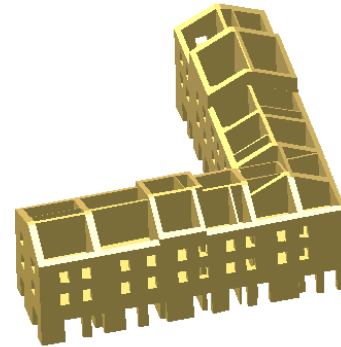
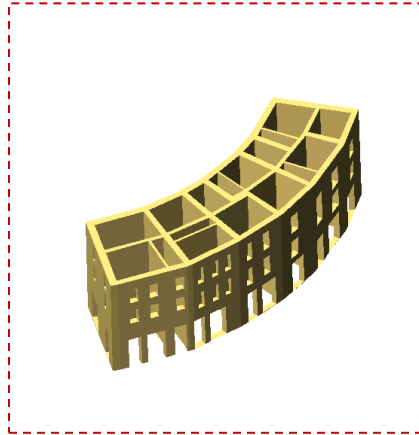
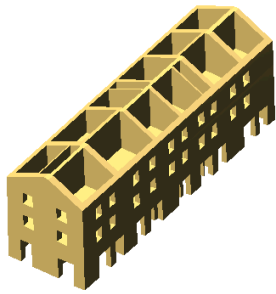
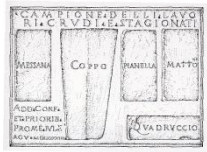
Borghi collinari a sviluppo circolare e lineare

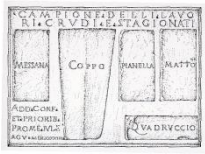
Vulnerabilità sismica alla scala urbana

Citerna (PG), 26 aprile 1917

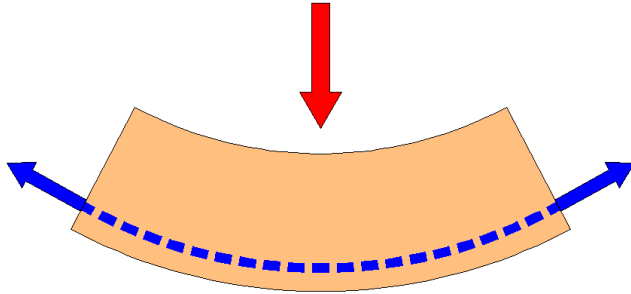




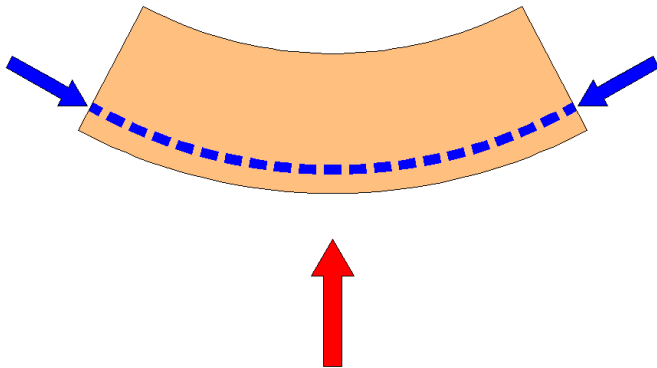




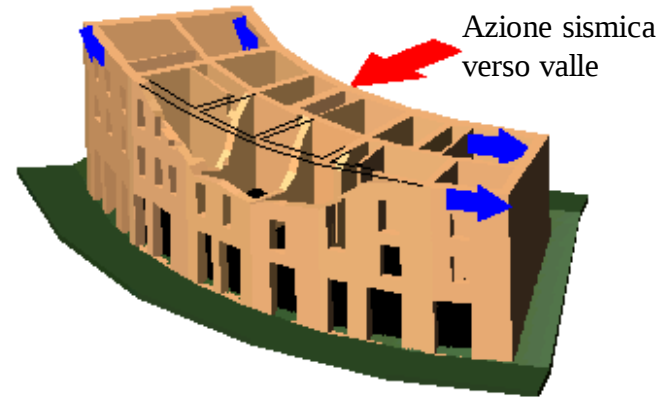
Effetti del sisma ortogonale negli isolati ad impianto curvilineo



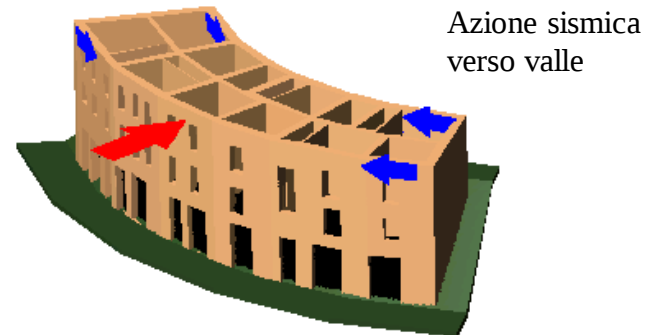
L'azione sismica verso valle mette in trazione la parete di facciata ((Allentamento parete di valle)



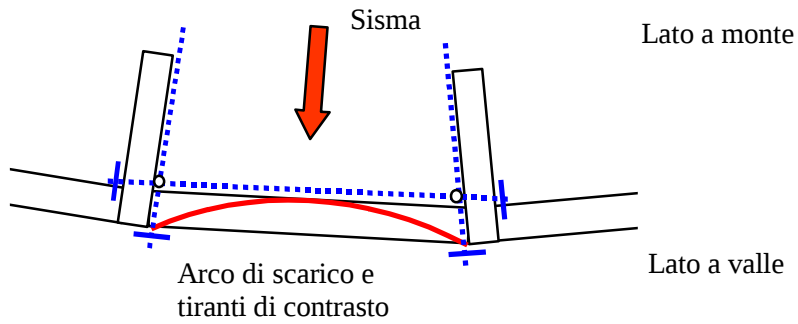
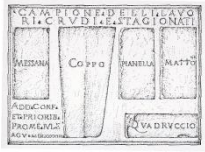
L'azione sismica verso monte comprime le pareti di facciata (Effetto arco)



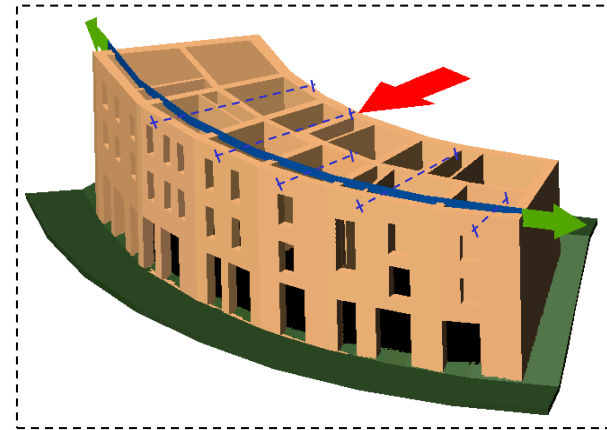
Azione sismica verso valle



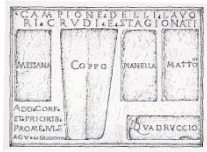
Azione sismica verso valle



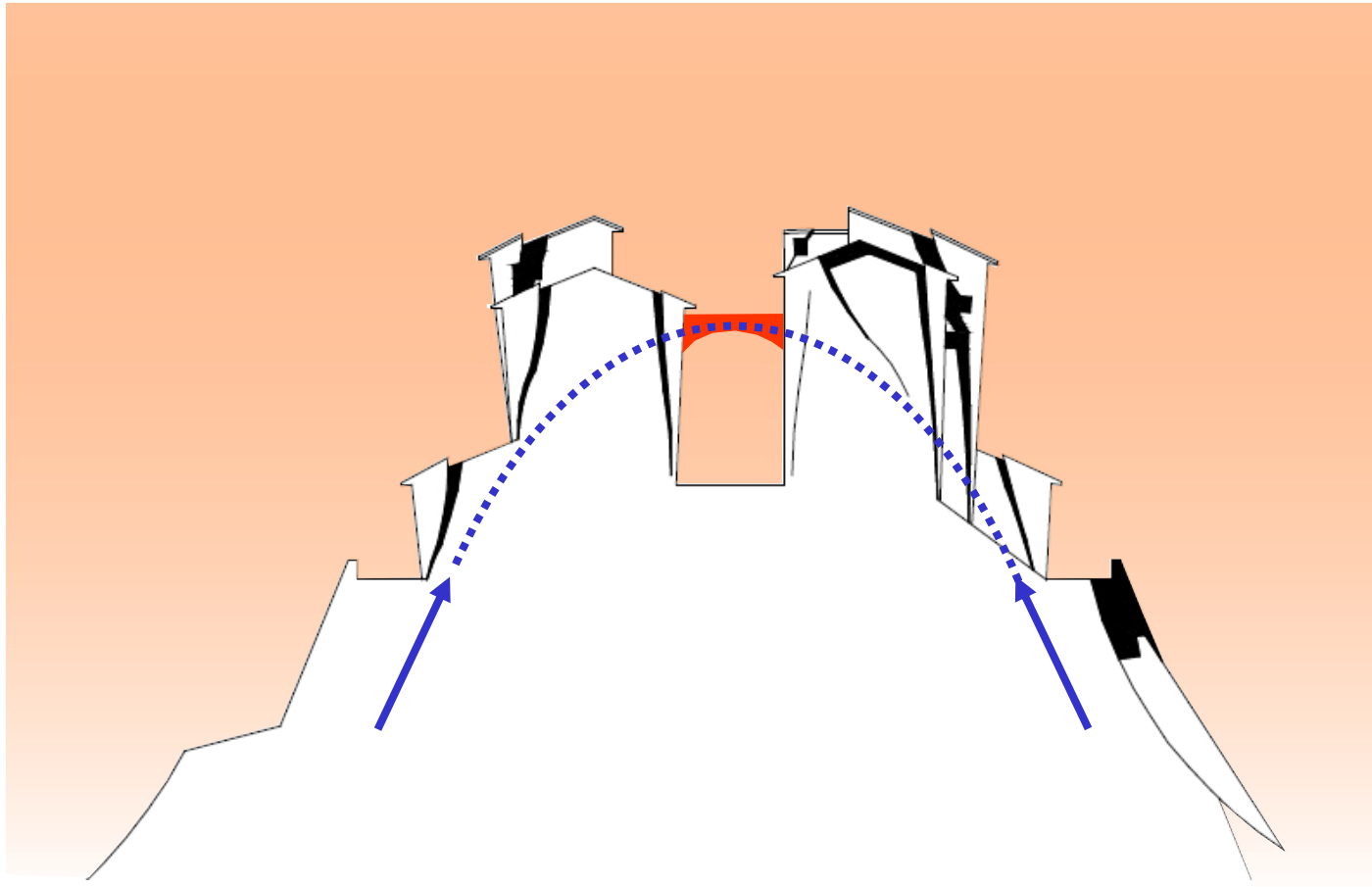
Azione sismica sulla singola parete con meccanismo resistente locale

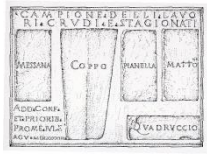


Meccanismo resistente assicurato da collegamenti metallici sommitali e di piano

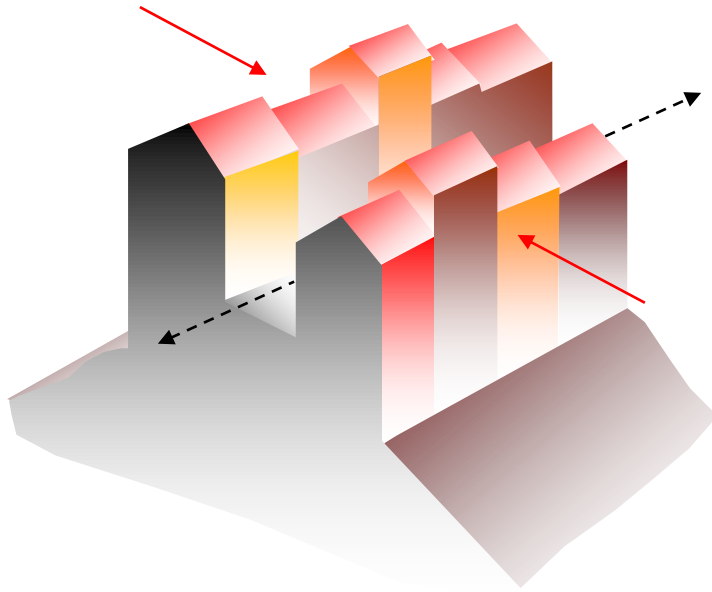


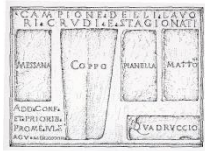
Meccanismi resistenti alla scala urbana



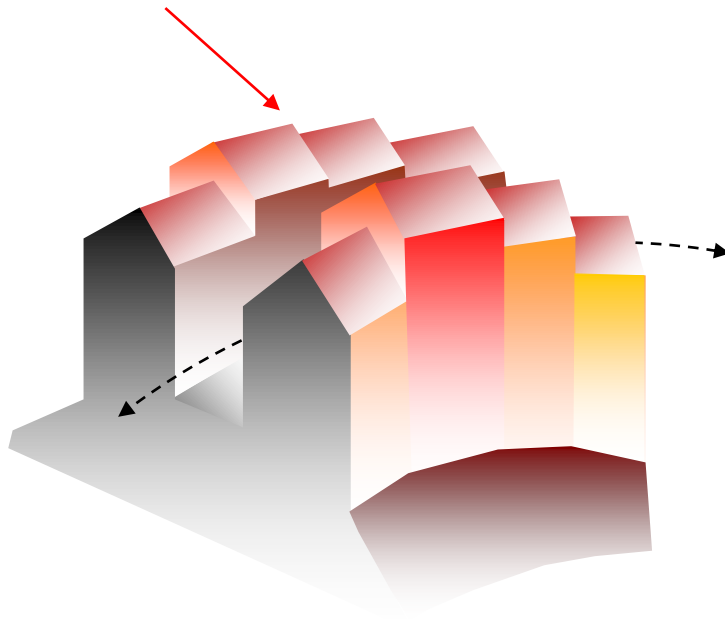


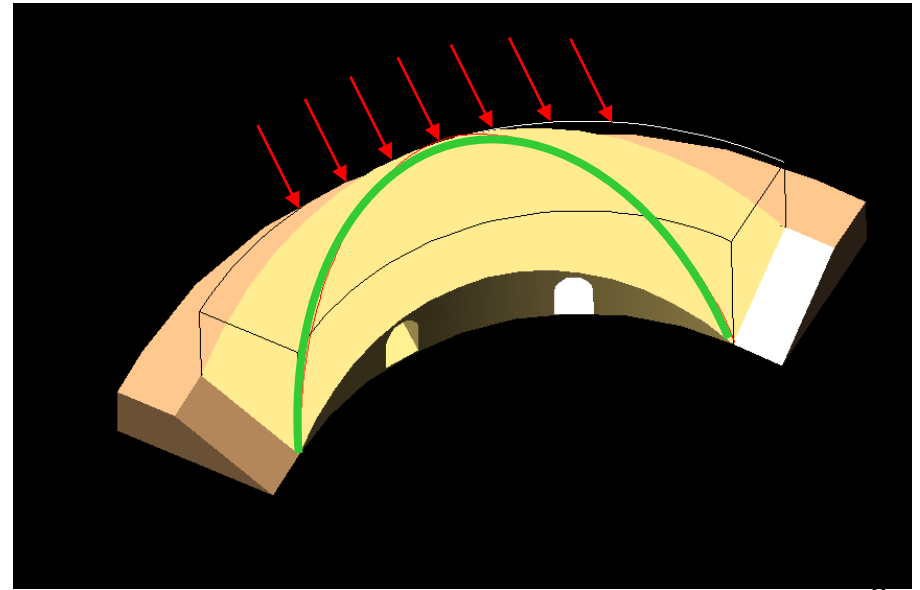
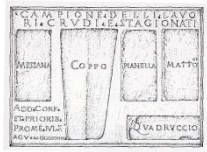
Valutazione del rischio sismico alla scala urbana

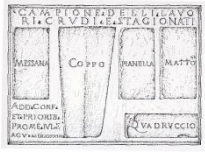




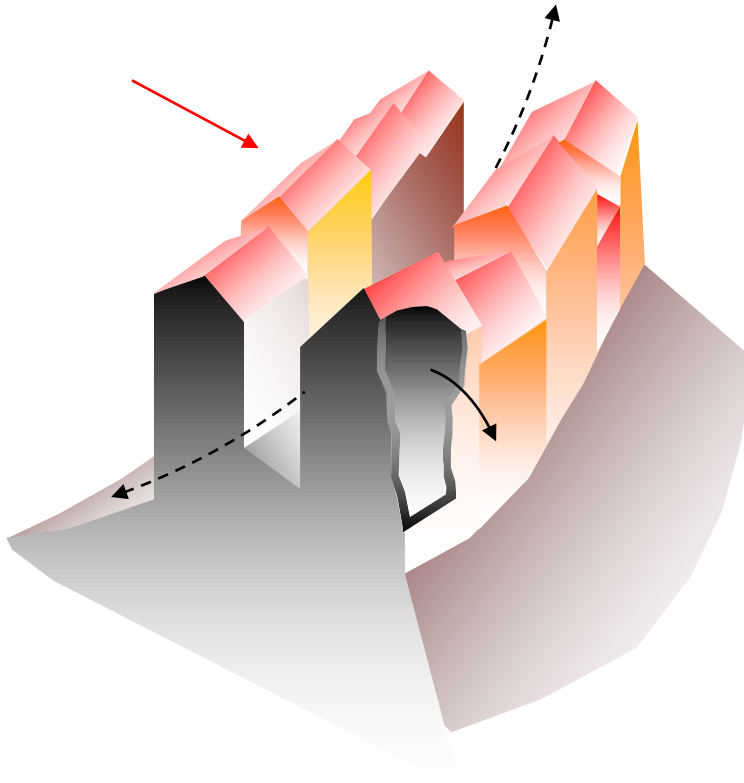
Valutazione del rischio sismico alla scala urbana

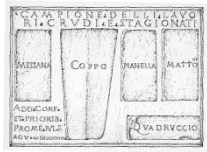




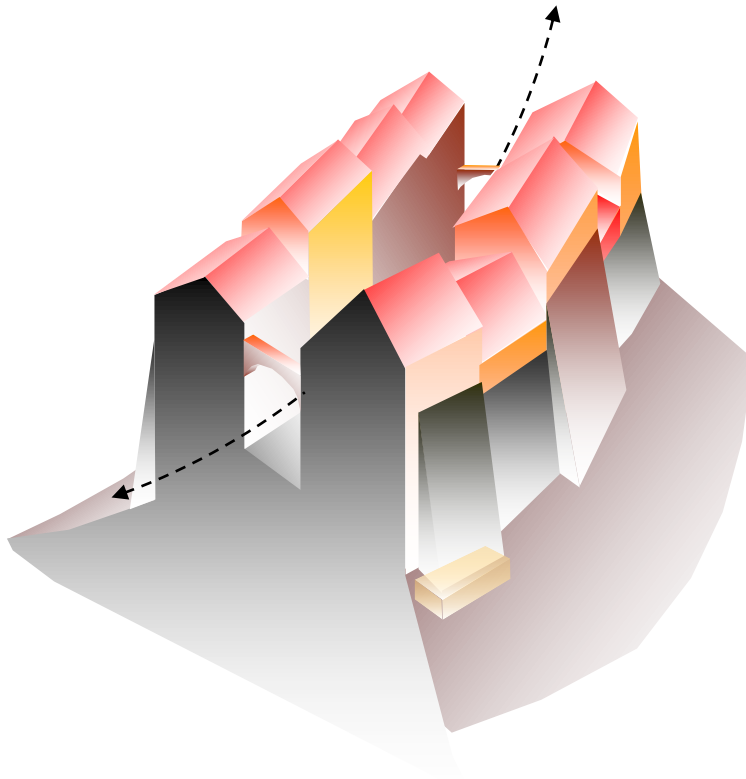


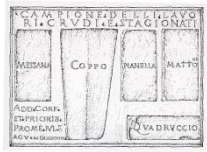
Valutazione del rischio sismico alla scala urbana



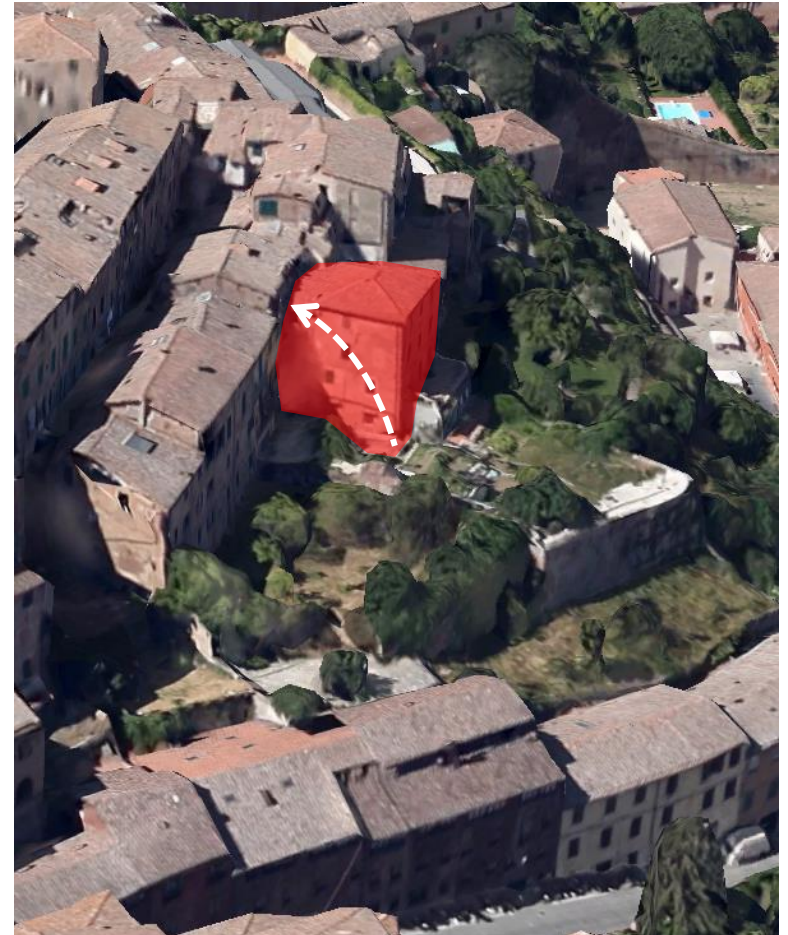
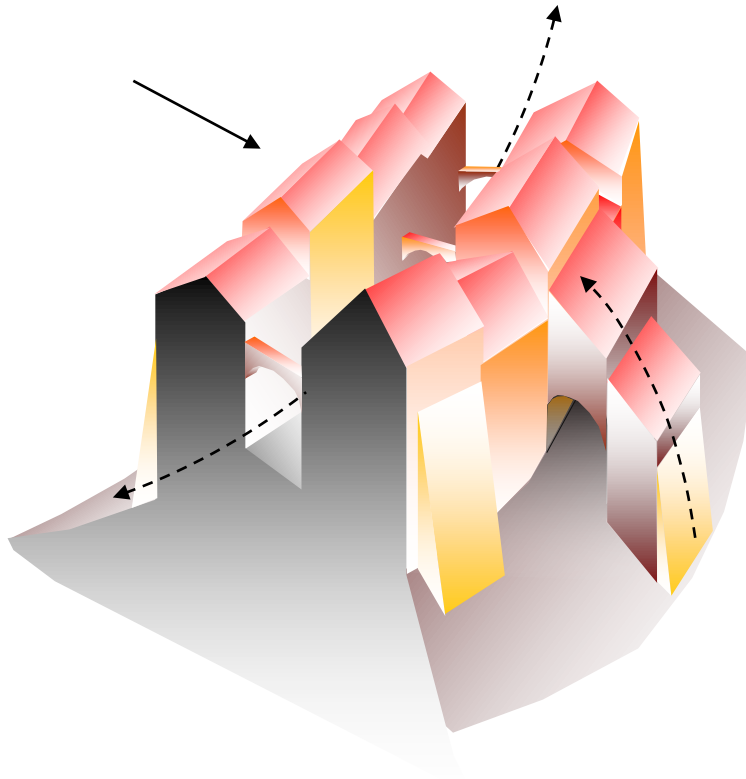


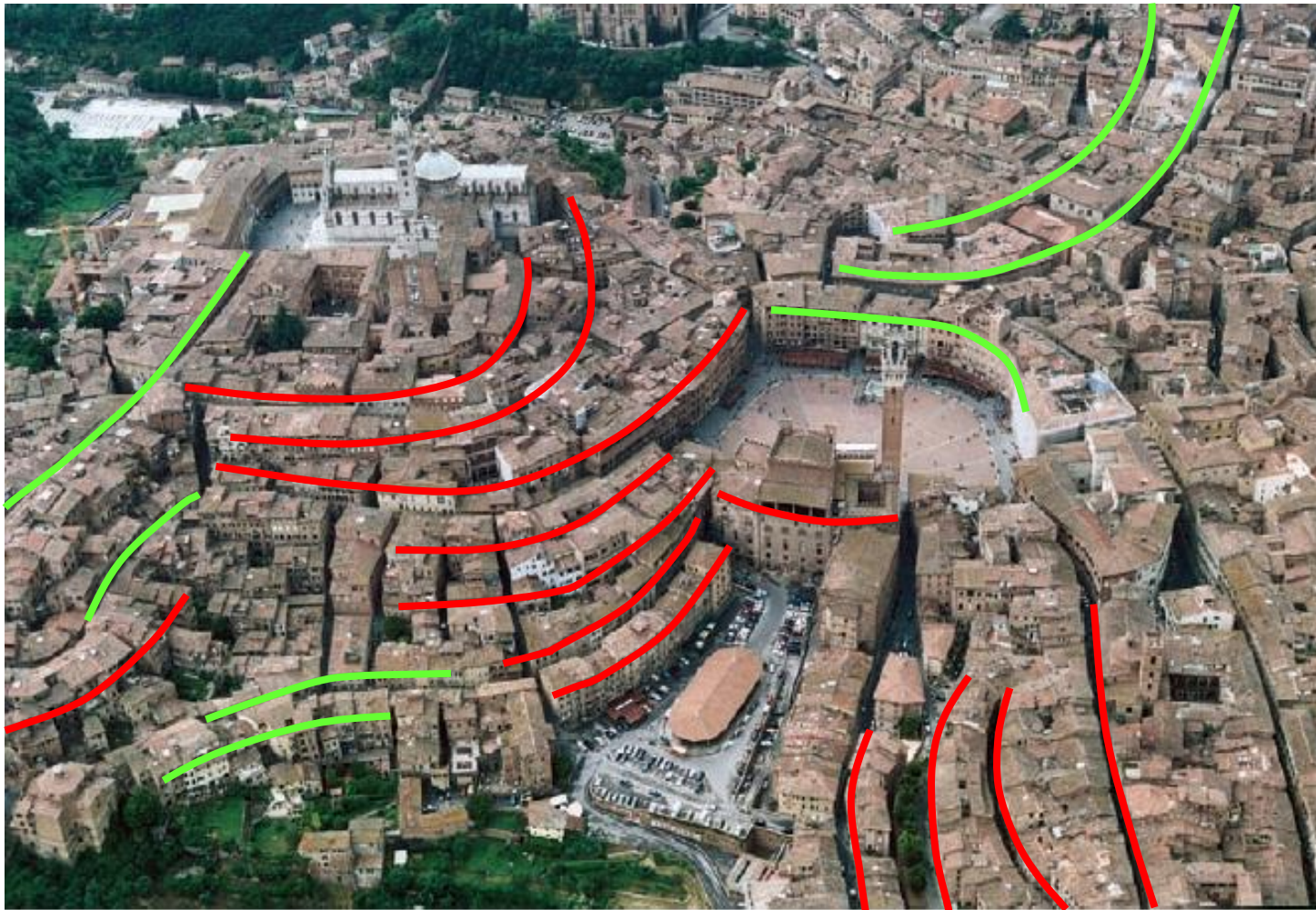
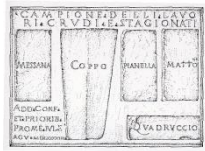
Valutazione del rischio sismico alla scala urbana



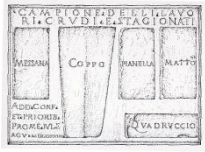


Valutazione del rischio sismico alla scala urbana

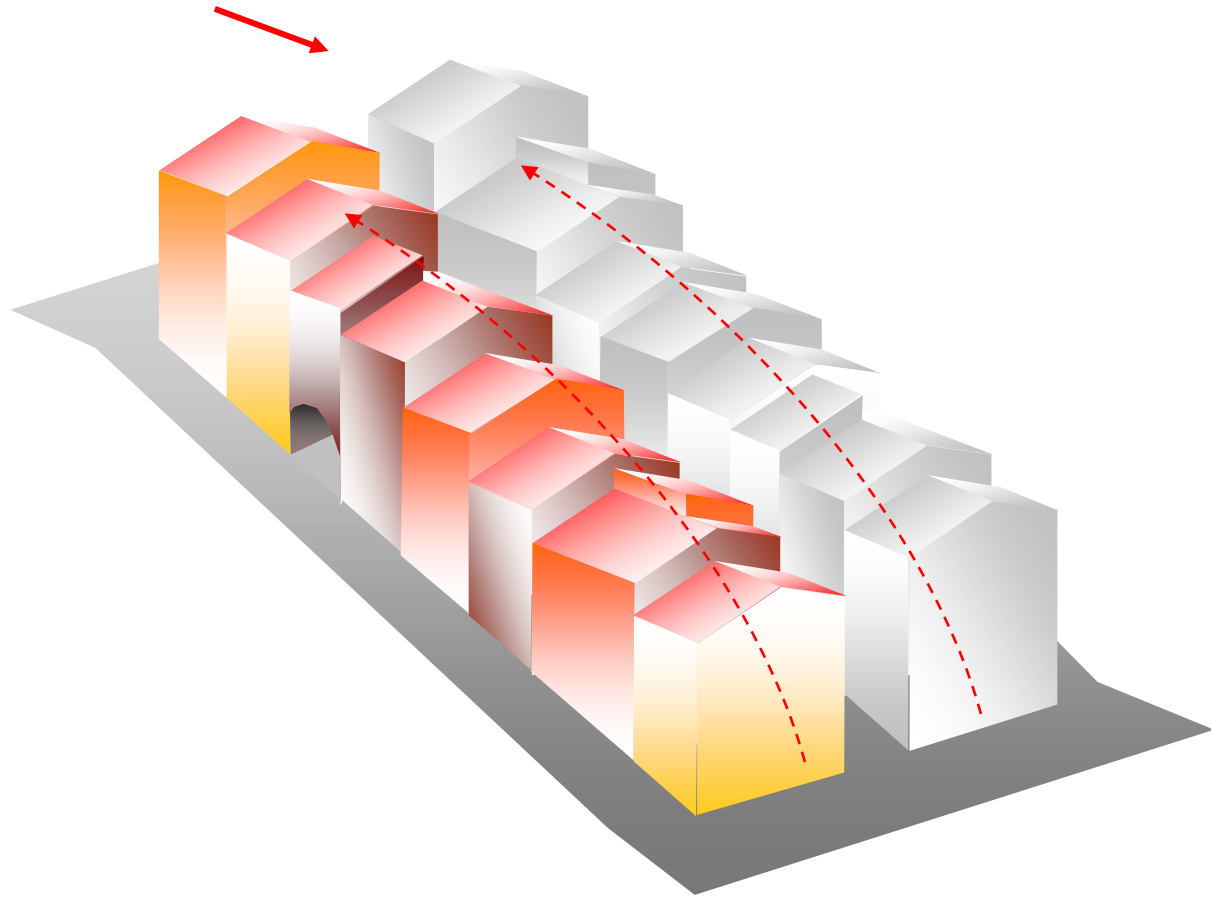


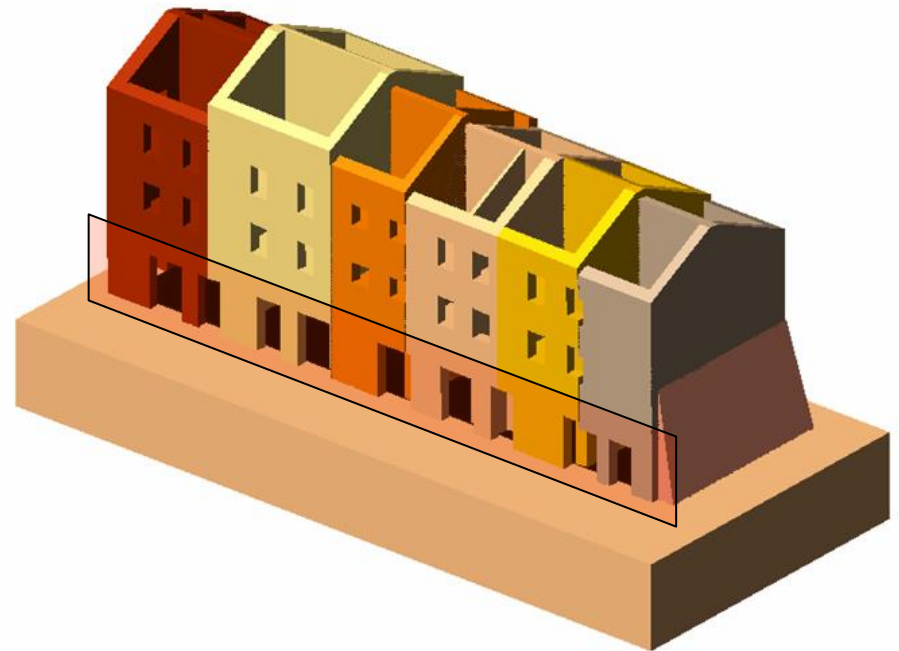
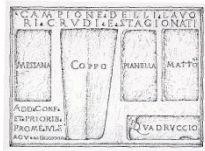


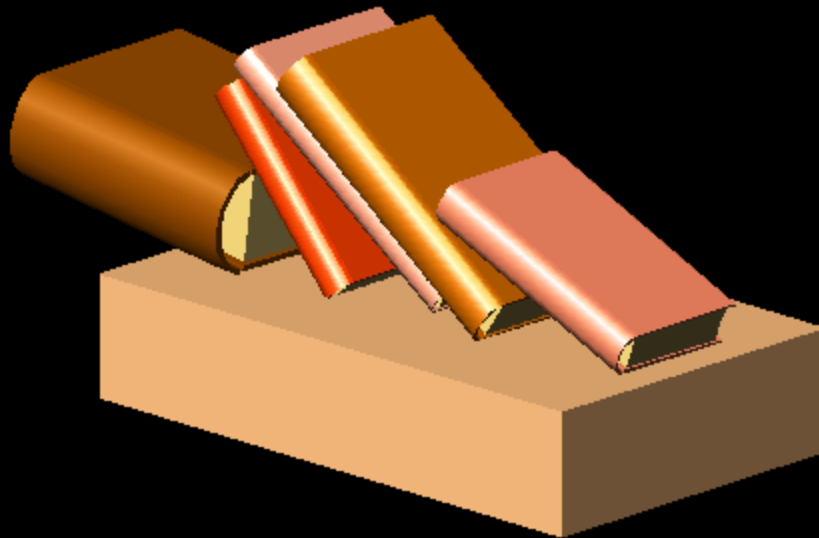
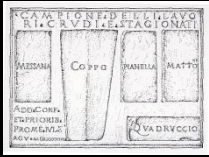
Siena: criticità determinate dalla conformazione planimetrica degli aggregati edilizi in relazione alla configurazione di pendio (concavità e convessità del lato a valle)

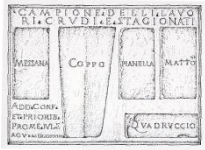


Valutazione del rischio sismico alla scala urbana

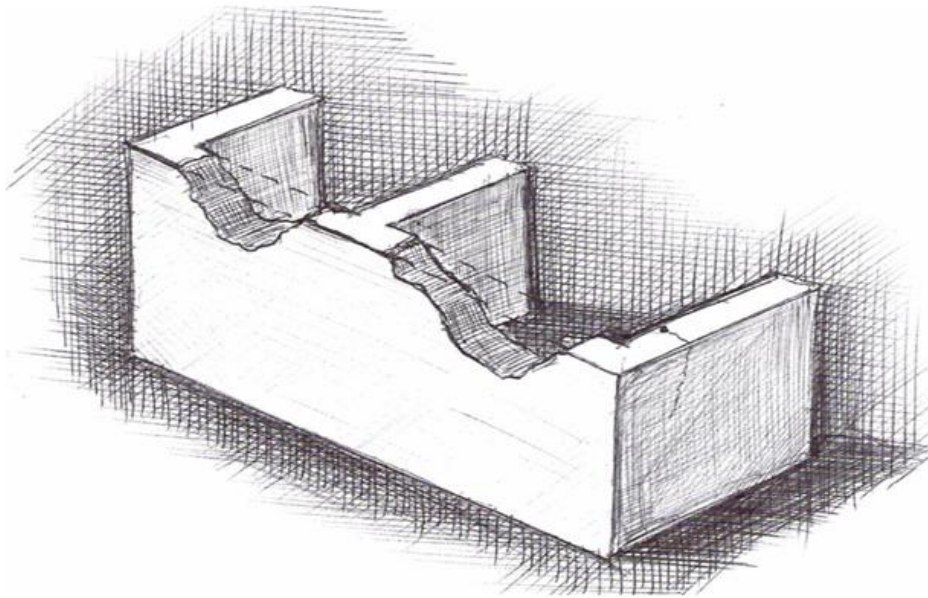
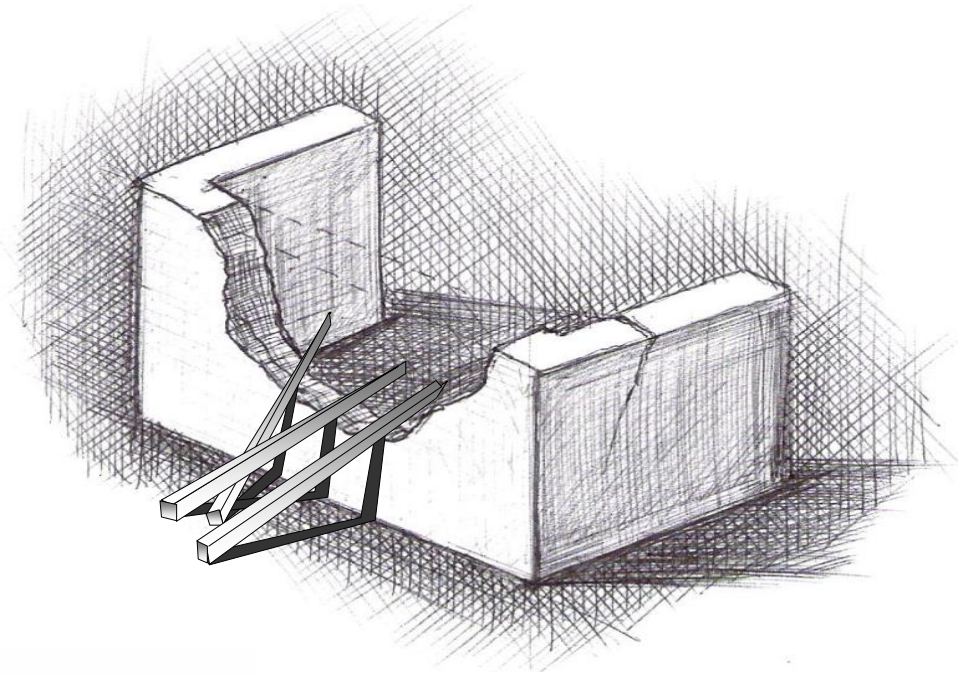
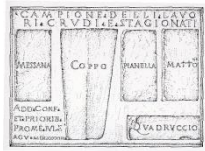


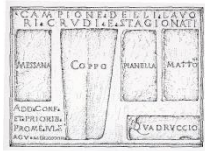




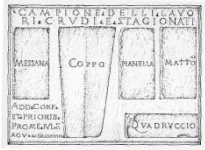


L'Aquila – 6 aprile 2009

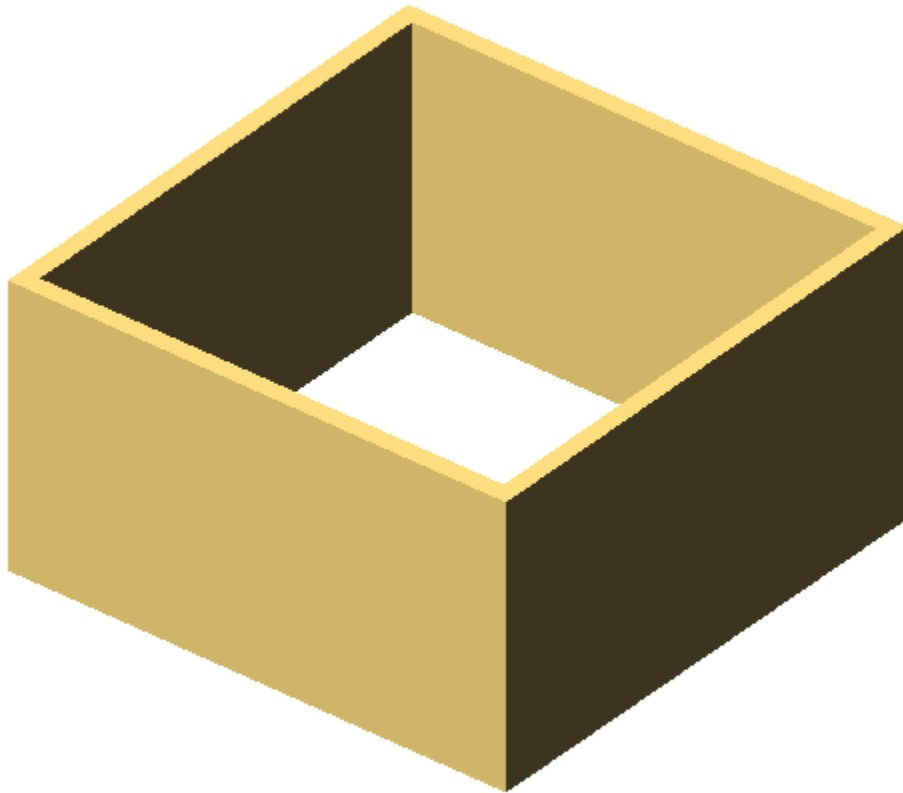
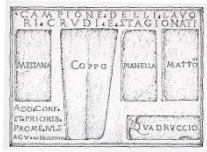


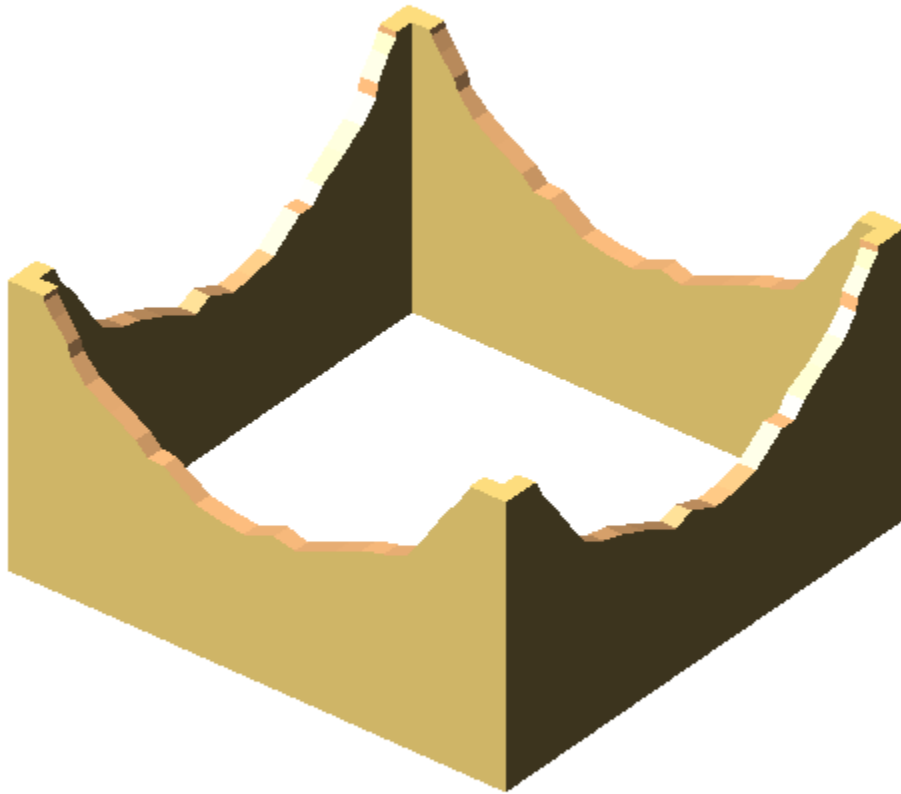
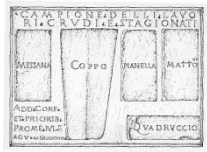


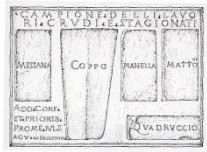
Terremoto dell'Emilia (maggio 2012):
ribaltamento di pareti sollecitate da azioni ortogonali



Camillo Ricci
(Terremoto di Argenta, 1624)



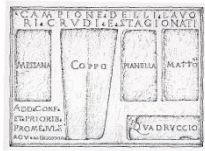


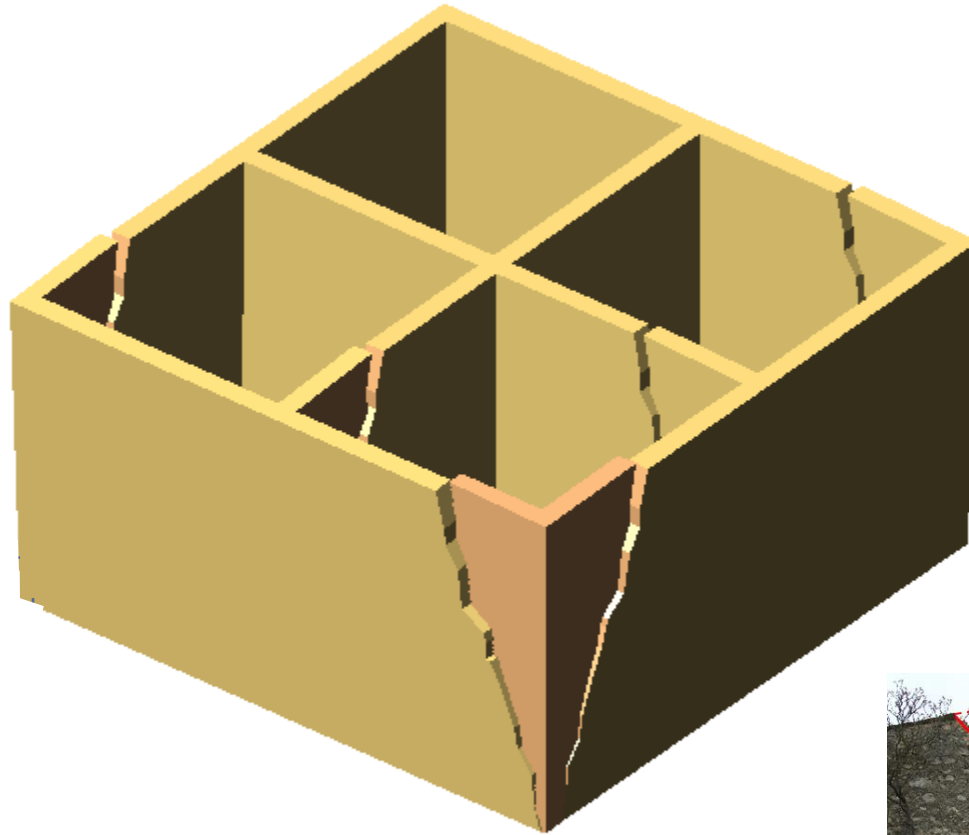


Umm al Jimal (Giordania), 749 dC



Chiesa di San Francesco - Avezzano (1915)







Torre di Babele



Ziqqurat (Persia)



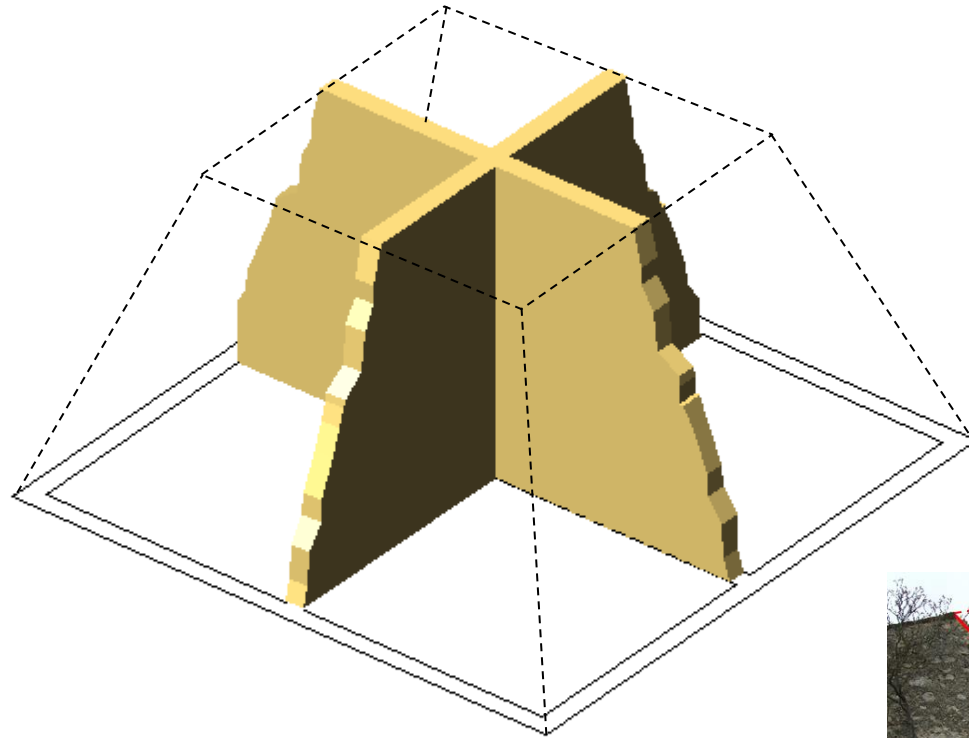
Piramidi egizie



Piramidi Maia



Castelli giapponesi





Torre di Babele



Ziqqurat (Persia)



Piramidi egizie



Piramidi Maia



Castelli giapponesi

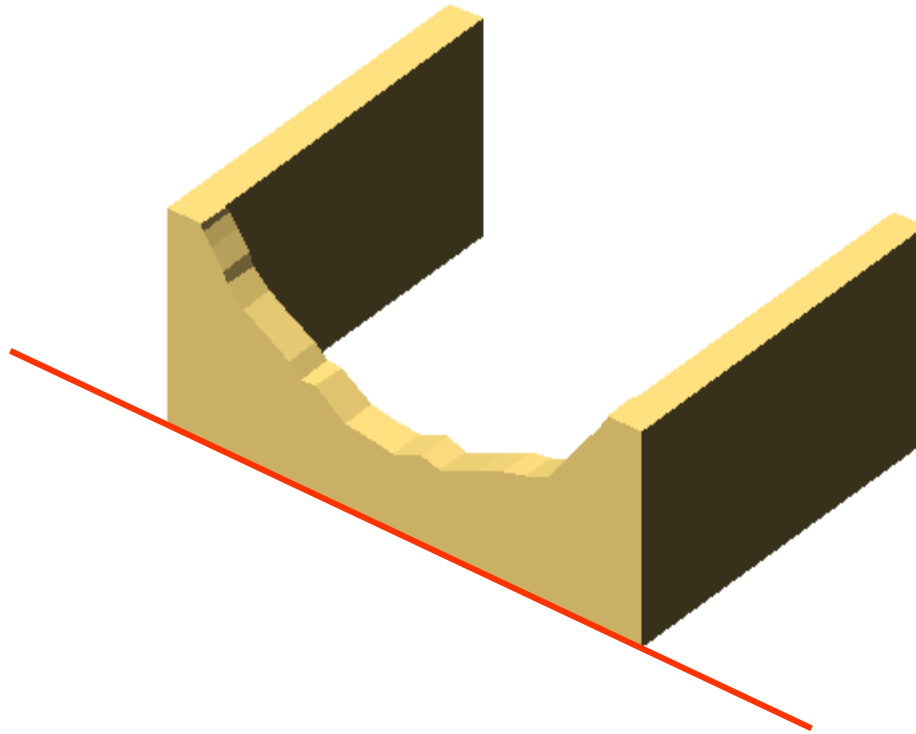
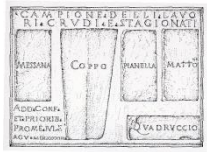


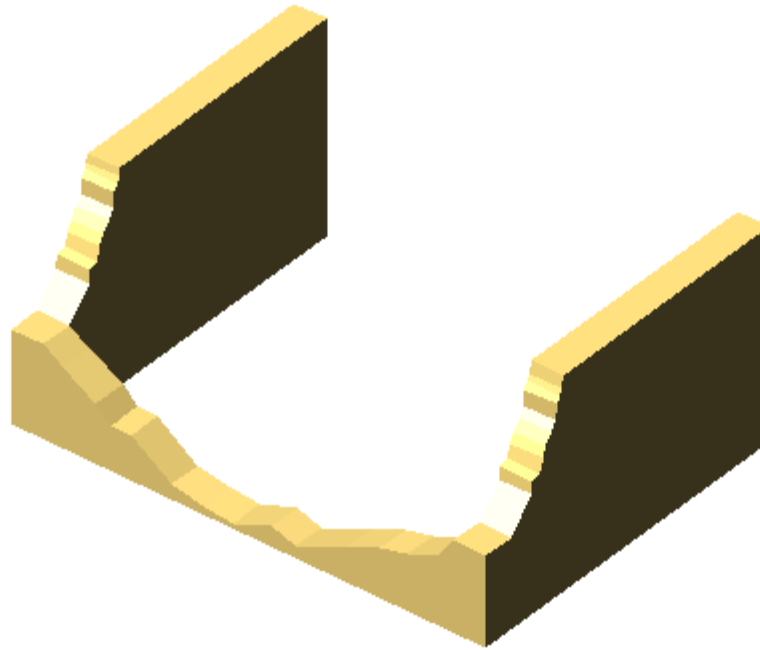
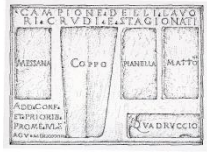
CD n° AC7

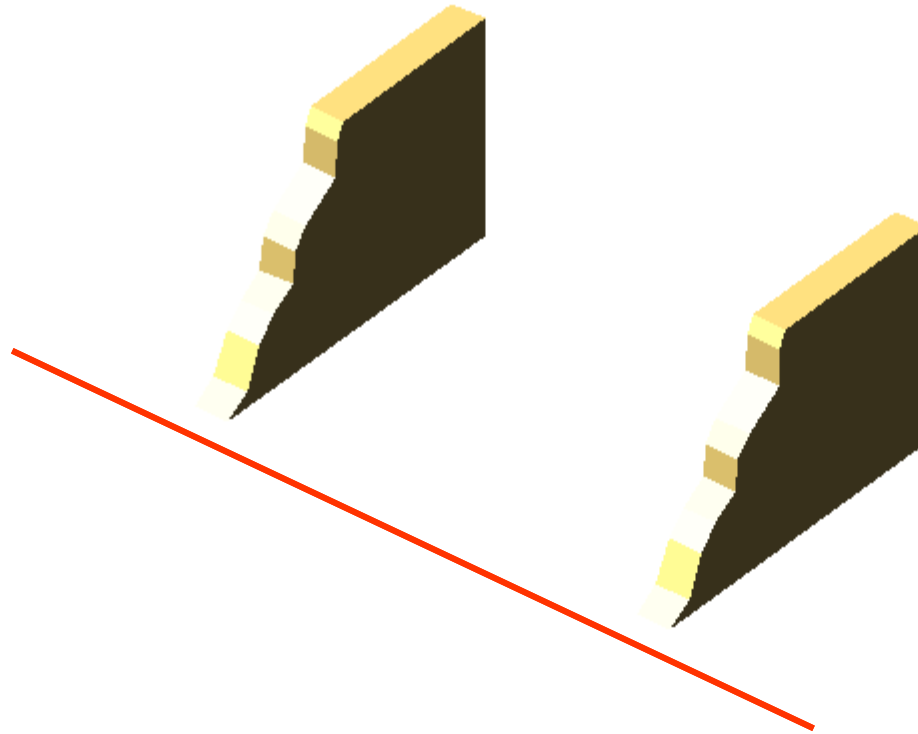
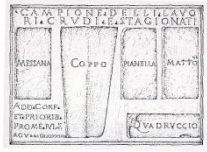
SOPRINTENDENZA ALLE ANTICHITA' DI OSTIA
Arch. Foto Soprint. - Nega. Serie B n. 2214/5 Inv. 4703

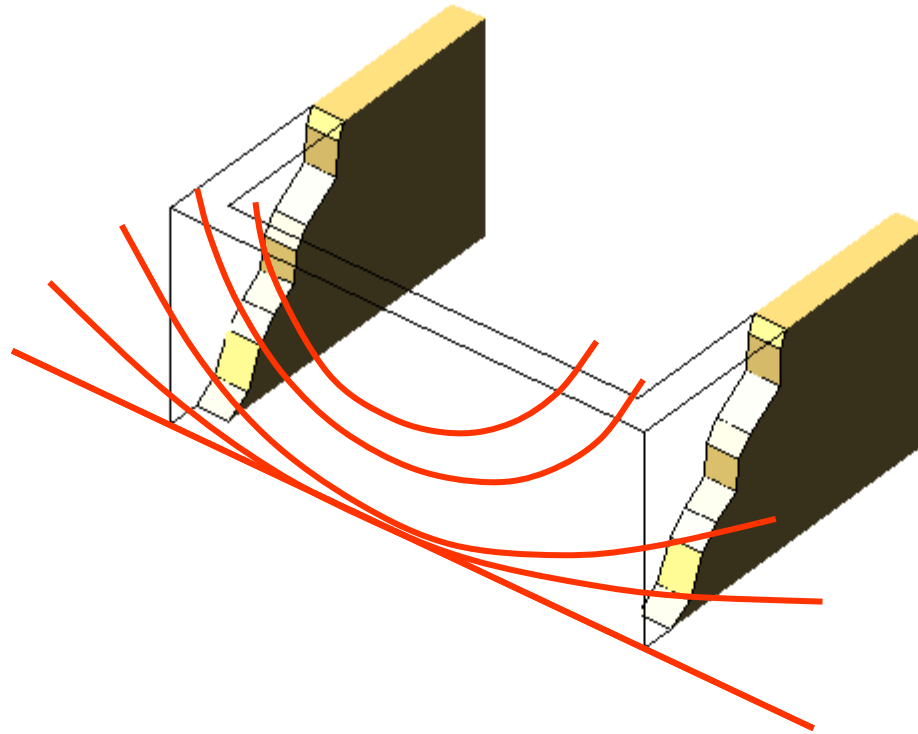
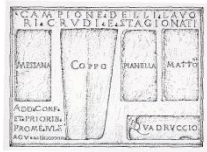


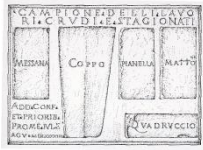
Via della Casa di Diana



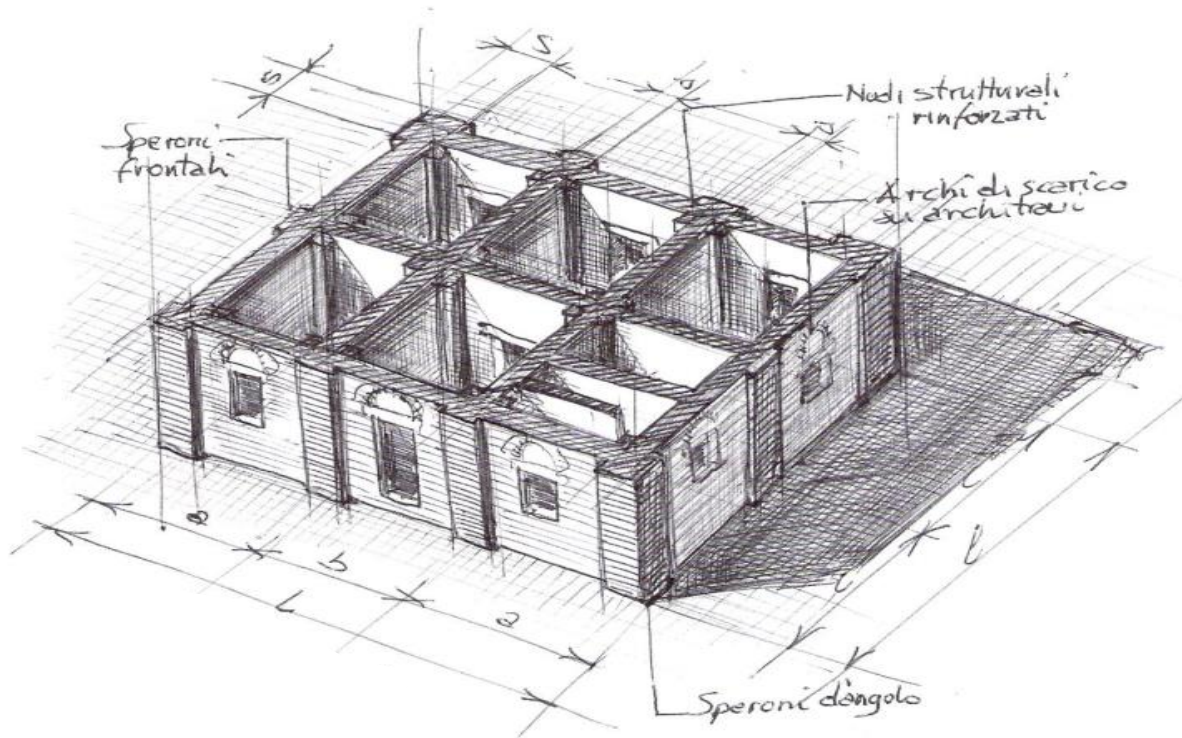






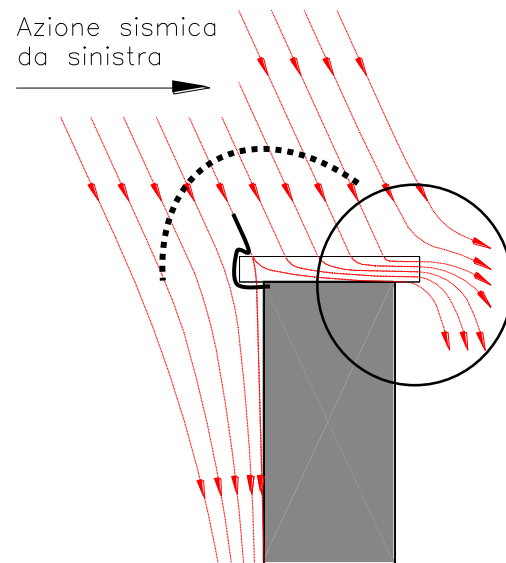
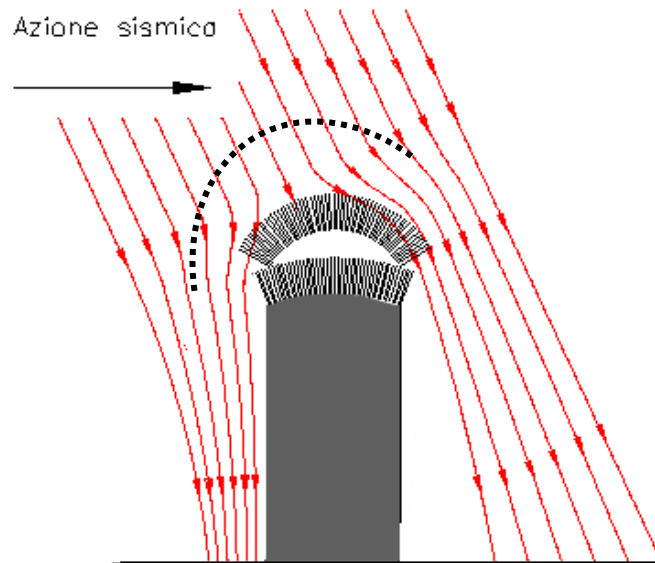
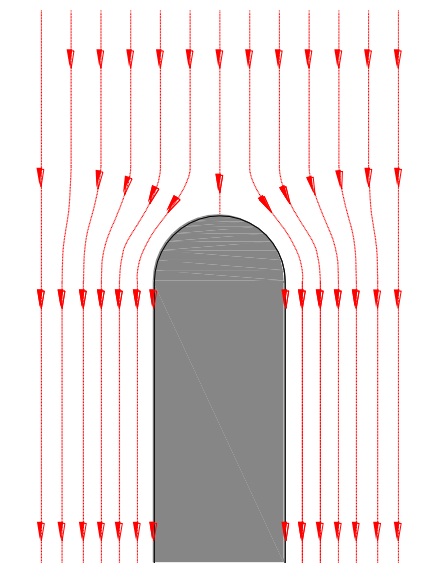


Progetto di “casa antisismica” elaborato dopo il terremoto del 1570 a Ferrara dall’architetto Pirro Ligorio, succeduto a Michelangelo presso la Fabbrica di San Pietro e trasferitosi alla corte degli Estensi nel 1568.



Punti fondamentali della “casa antisismica”:

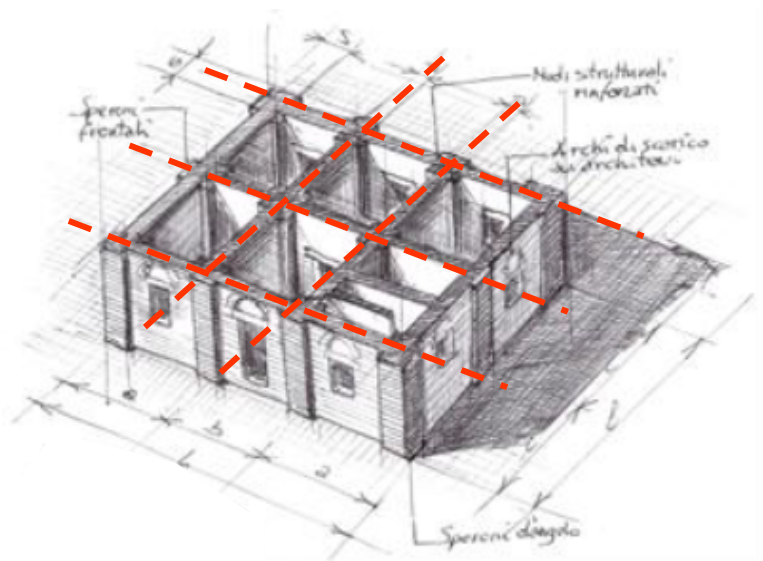
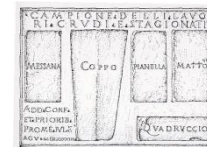
- regolarità in pianta;
- interassi contenuti fra i muri portanti;
- spessori consistenti delle murature;
- cantonali rinforzati;
- rinforzo degli incroci murari;
- ordinata disposizione delle aperture;
- presenza di archi di scarico sopra gli architravi.



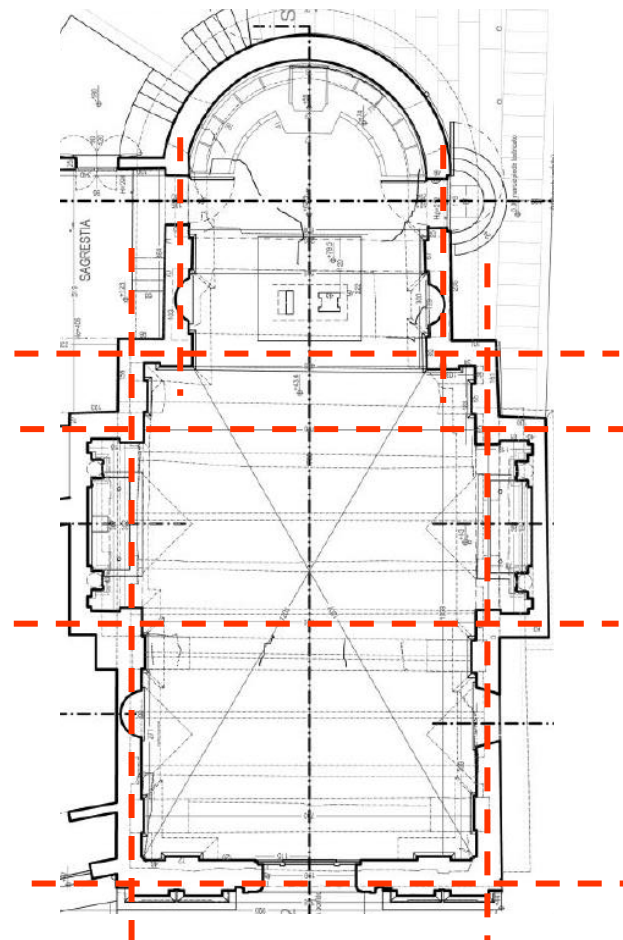
Archi di parete predisposti per diffondere i flussi di compressione in condizioni statiche e sismiche in presenza di archi e anomalie prodotte dagli architravi

Pirro Ligorio
di una casa antisismica

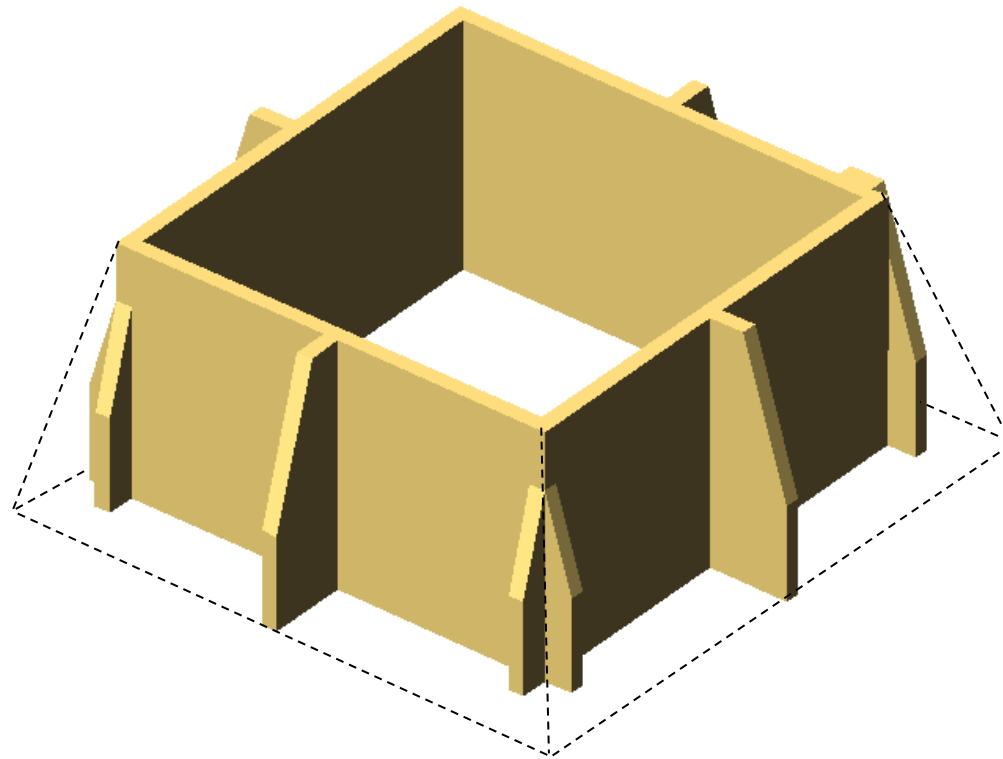
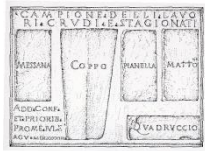
Progetto
Ferrara - 1574



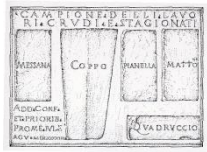
VALENTINA BARONCINI architetto
via Giuseppe Martucci 10
40136 BOLOGNA
Tel.-fax: 051/580817 cell. 338/9211687
valentina.baroncini@tiscali.it
valentina.baroncini@archiworldpec.it
CF. BRNVNT70P64A944K
P. IVA 03105041200

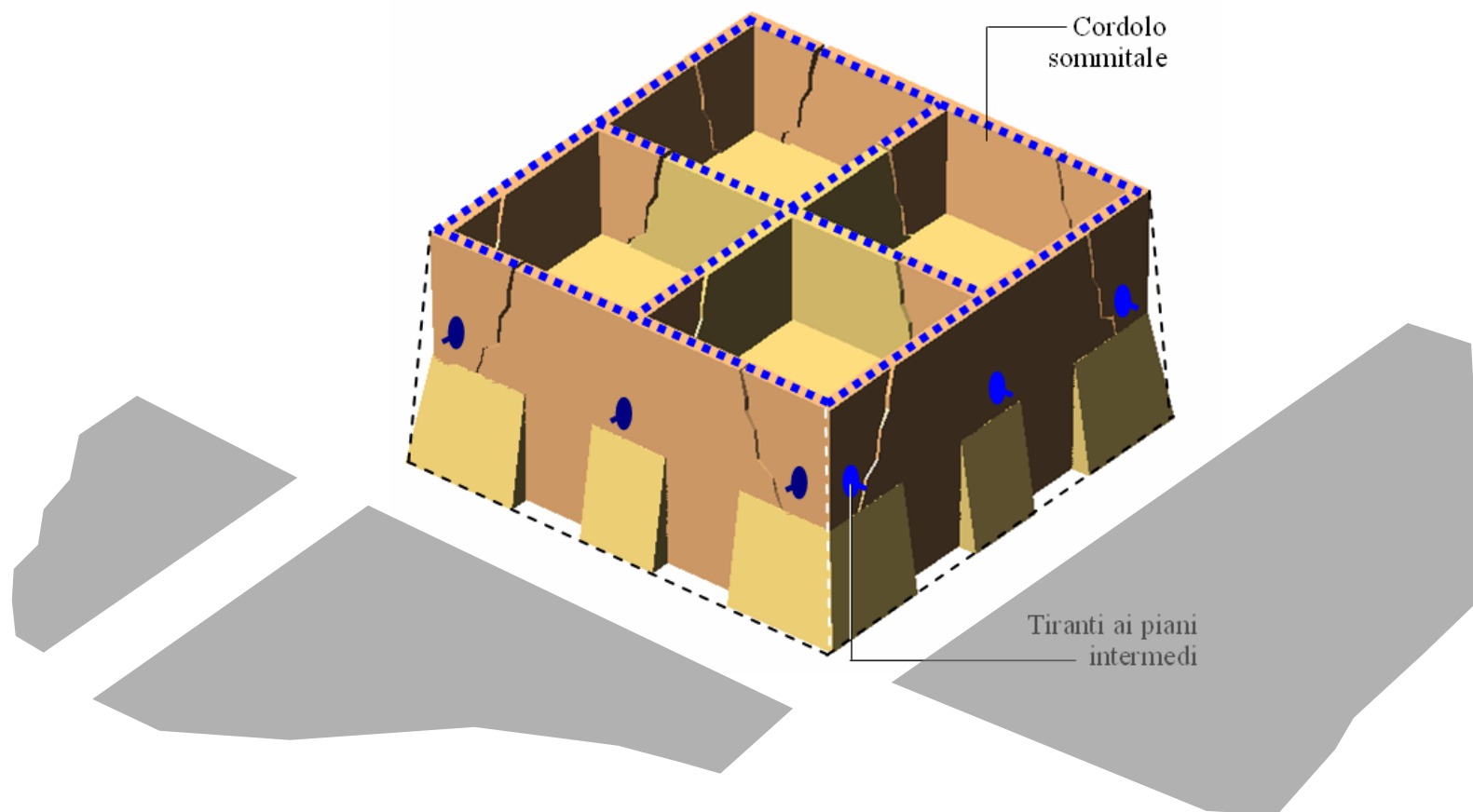
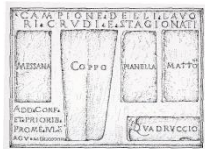


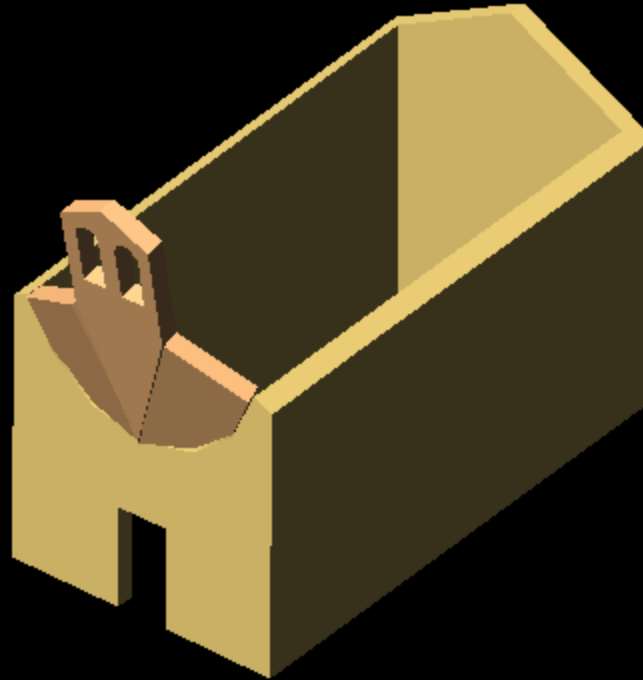
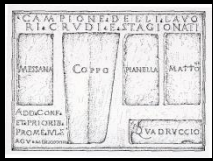
ORATORIO DI SANTA CROCE
SAN FELICE SUL PANARO (MO)



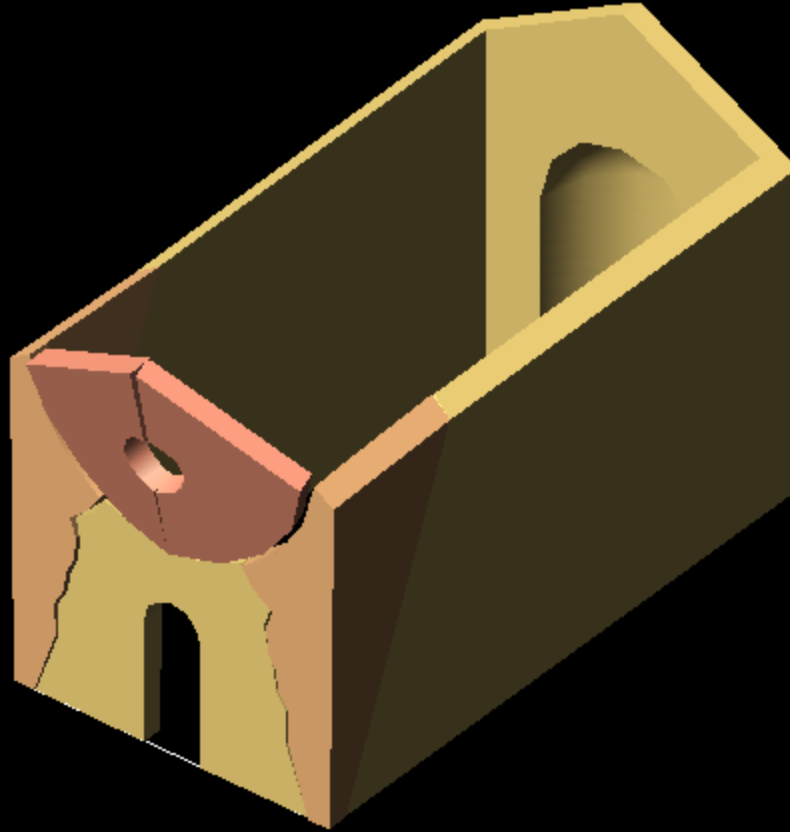
Lo stesso principio!

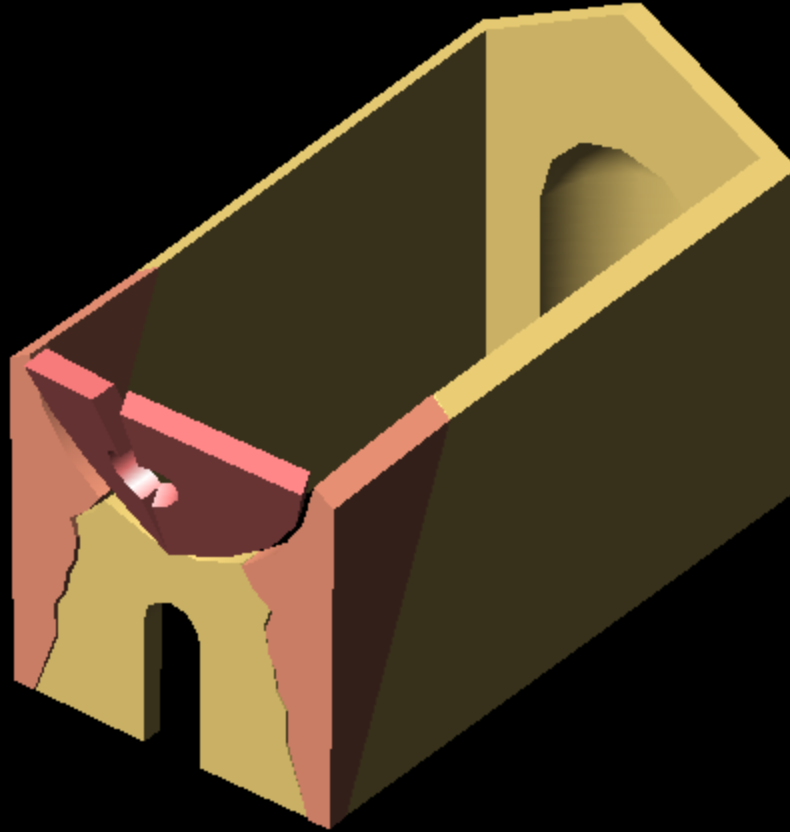
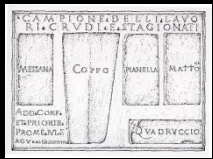


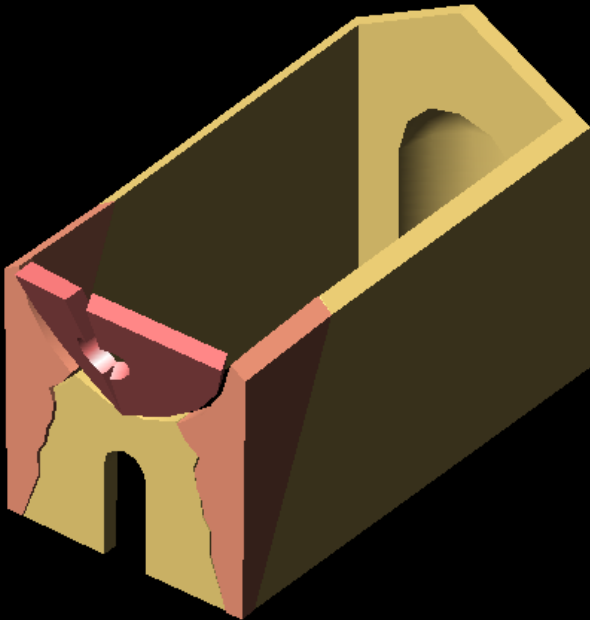
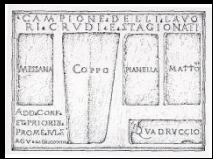


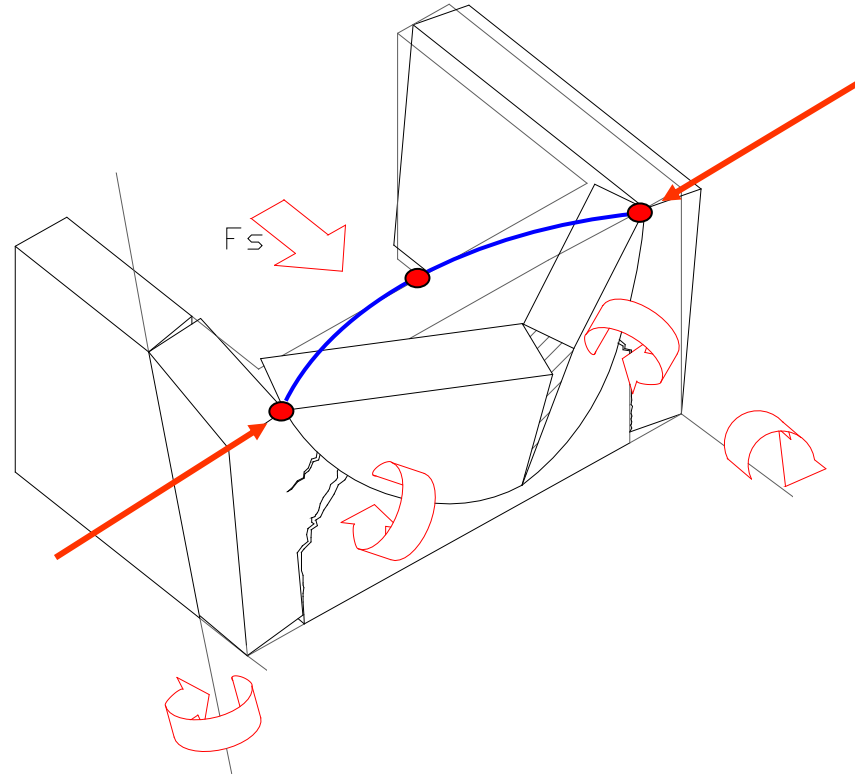
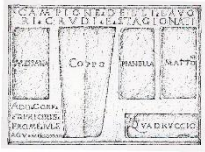


Cinematismi di danno tipici delle chiese a navata unica

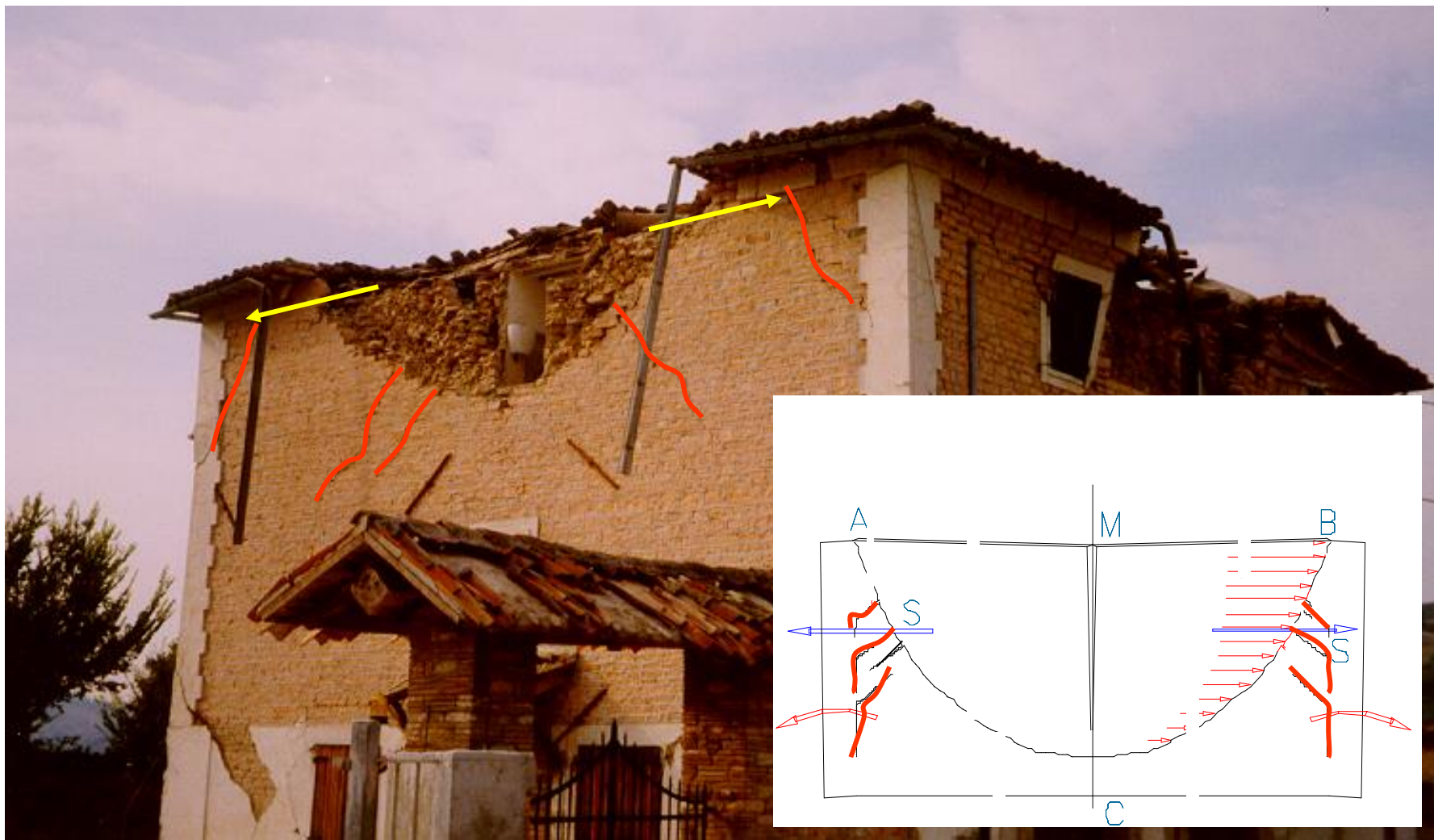






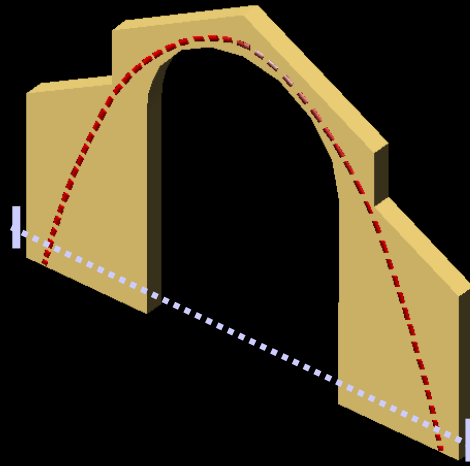


Ribaltamento pareti sollecitate da azioni ortogonali

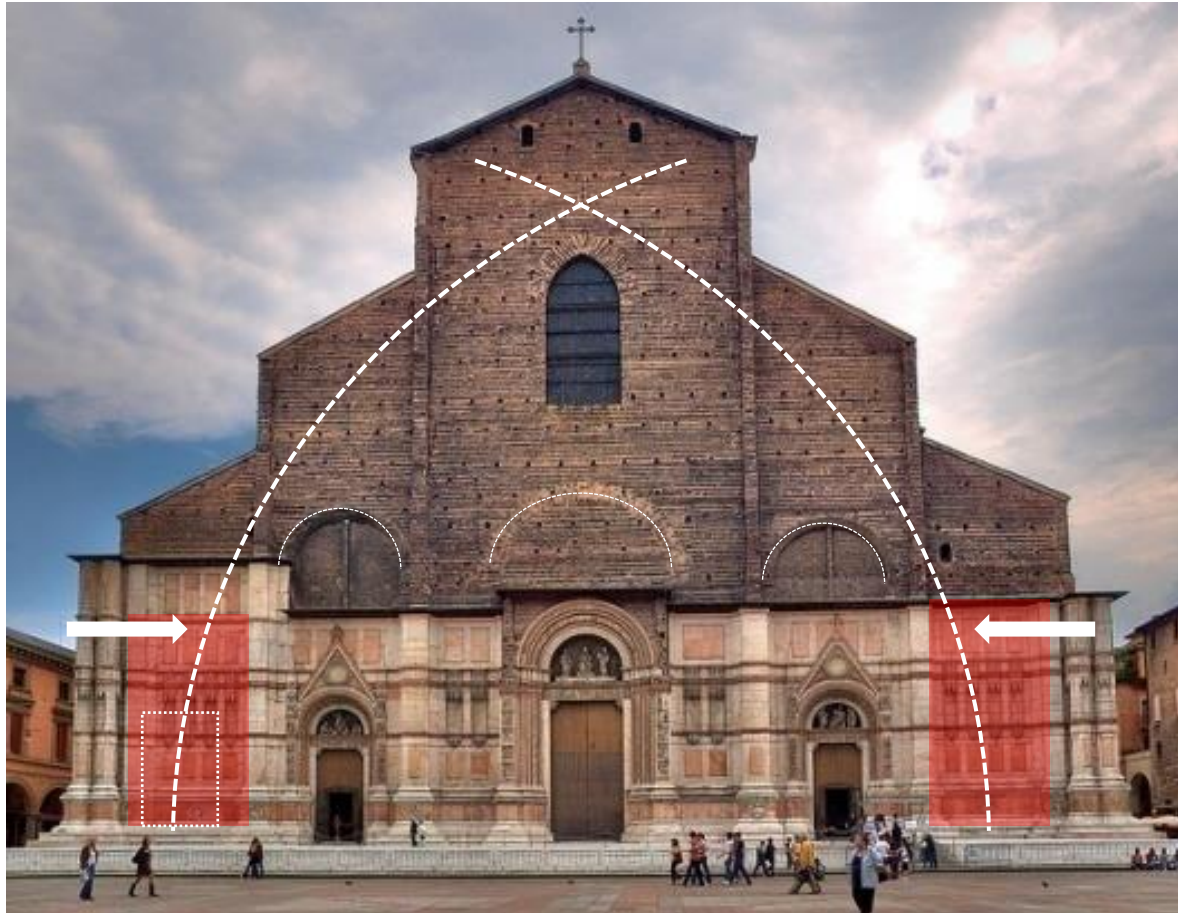
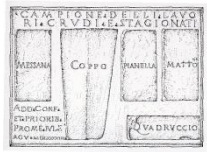


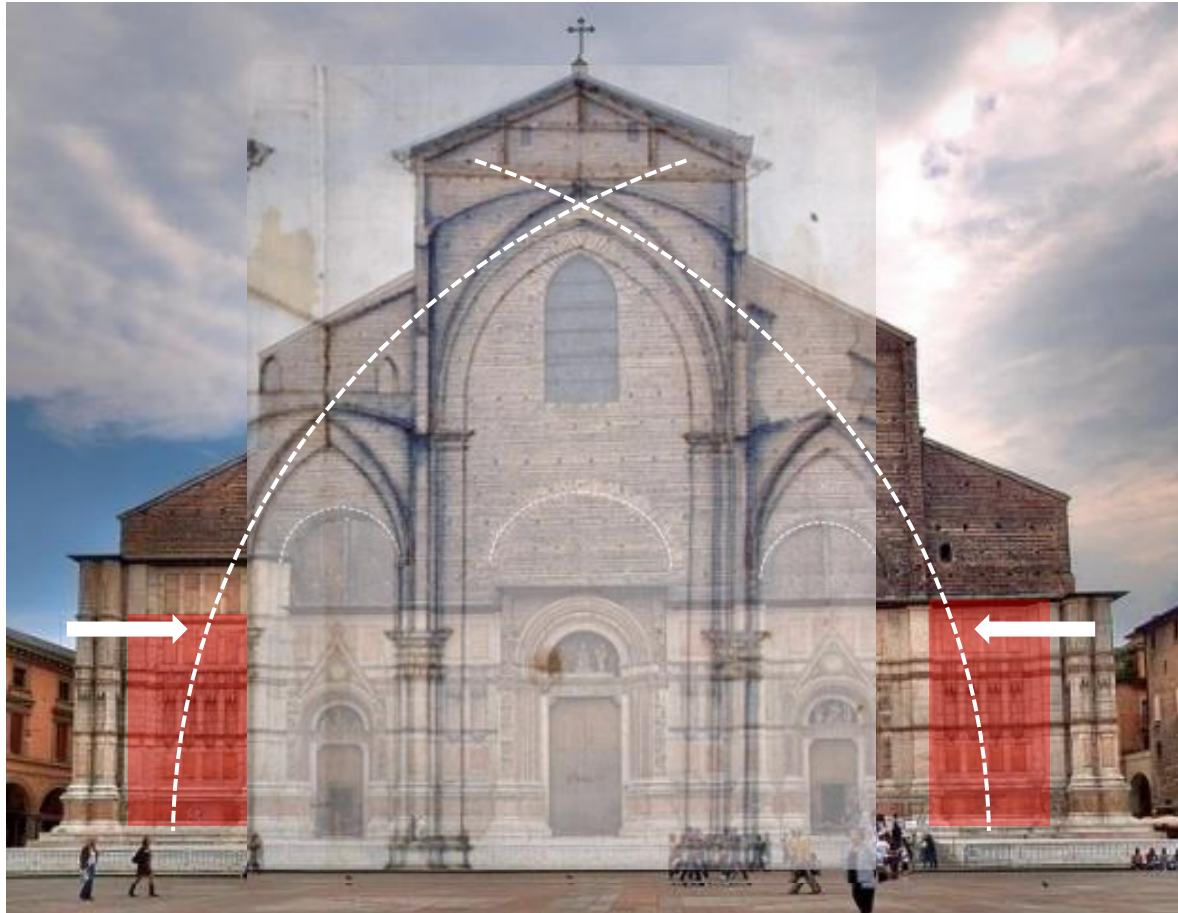
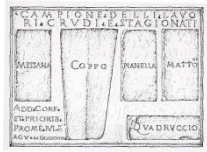
Edificio di Sellano (PG) danneggiato dal sisma del 1997

Foto Ing. A. Anastasi



Cinematismi di danno tipici
delle chiese a navata unica







Cinematismi di danno tipici
chiese a navata unica

delle



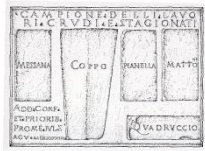
Cinematismi di danno tipici
chiese a navata unica

delle

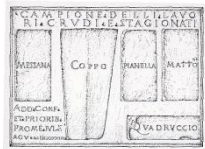


Cinematismi di danno tipici
chiese a navata unica

delle



Vetulonia



Rilievo critico

Ministero delle Infrastrutture
Ministero dell'Interno
Dipartimento di Protezione Civile

PROCEDURE PER LA VALUTAZIONE DELLA
SICUREZZA E LA REDAZIONE DEI PROGETTI

NUOVE NORME TECNICHE PER LE COSTRUZIONI

DM Infrastrutture 17 gennaio 2018

CAP. 8 - COSTRUZIONI ESISTENTI

8.5 – DEFINIZIONE DEL MODELLO DI RIFERIMENTO PER LE ANALISI

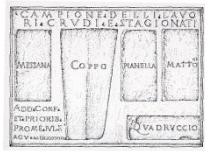
..... è impossibile prevedere regole specifiche per tutti i casi. Di conseguenza, **il modello per la valutazione della sicurezza dovrà essere definito e giustificato dal Progettista caso per caso**tenendo conto:

- dell'analisi storico-critica;

- del rilievo geometrico-strutturale;

- della caratterizzazione meccanica dei materiali

- del livello di conoscenza e fattori di confidenza

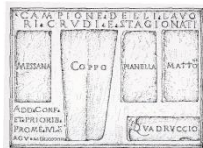


Tecniche costruttive e materiali da costruzione

Città di Castello

Evoluzione di una casa torre in
Corso V.Emanuele



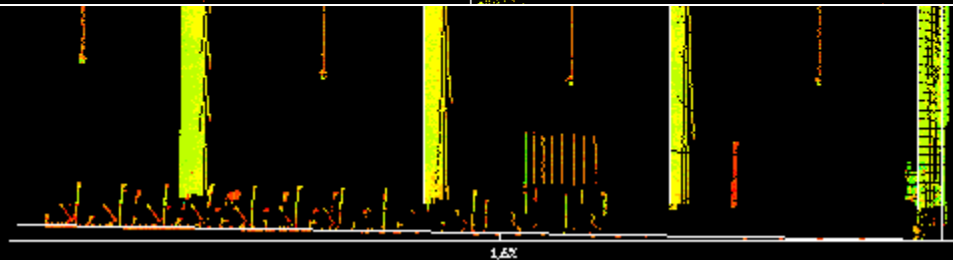
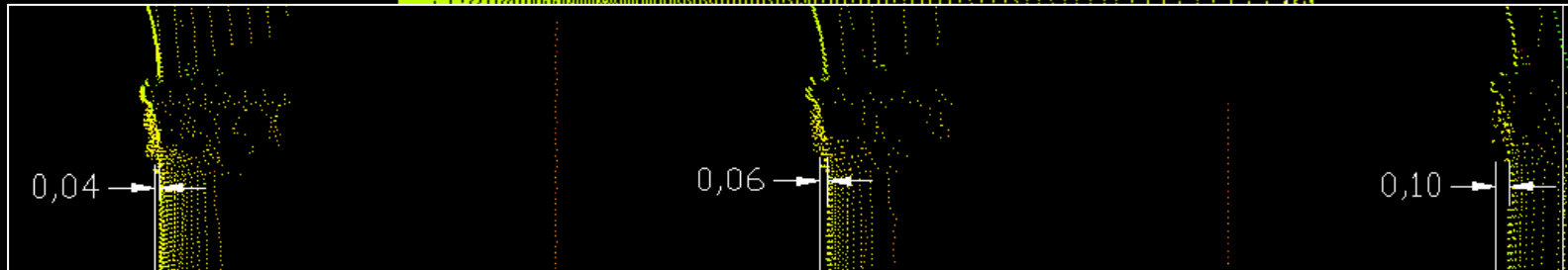
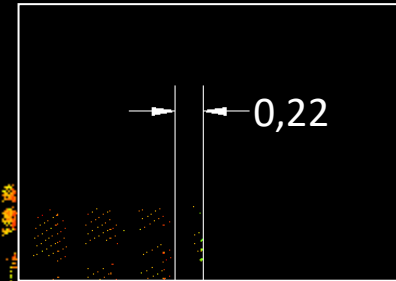
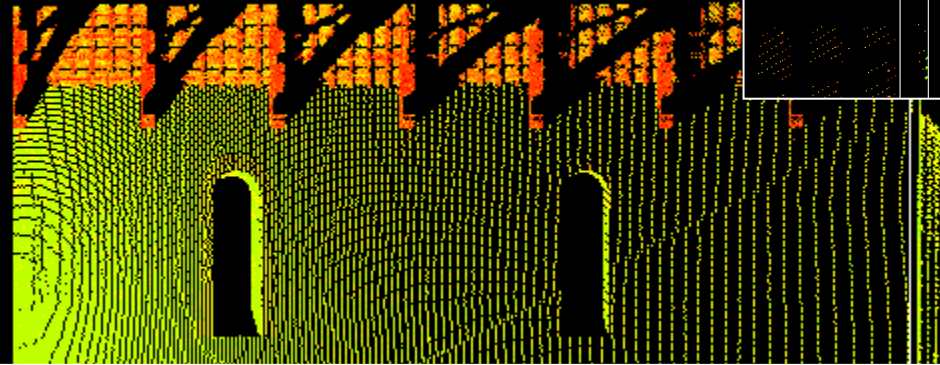


Pianta del Piano Terra

- | | | |
|------------------|----------------------|---------------------|
| ①
XI-XII Sec. | ③
XVII-XVIII Sec. | ⑤
XVIII-XIX Sec. |
| ②
XVII Sec. | ④
XVIII Sec. | ⑥
XIX-XX Sec. |







1917 Terremoto di Citerna-Monterchi

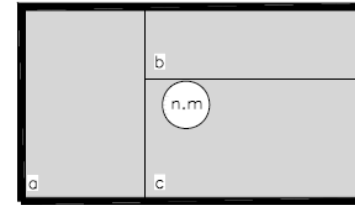
Atterrato il timpano della chiesa e scosse due ultime arcate della navata centrale sopra l'organo

Danneggiato il campanile (altre scosse nel 1919)

Segue demolizione della navata centrale – Rifacimento dei muri di sopraelevazione con le antiche finestre a feritoia

Demolito il tetto (ripristinato l'antico rosone di facciata)

Maglia tipo

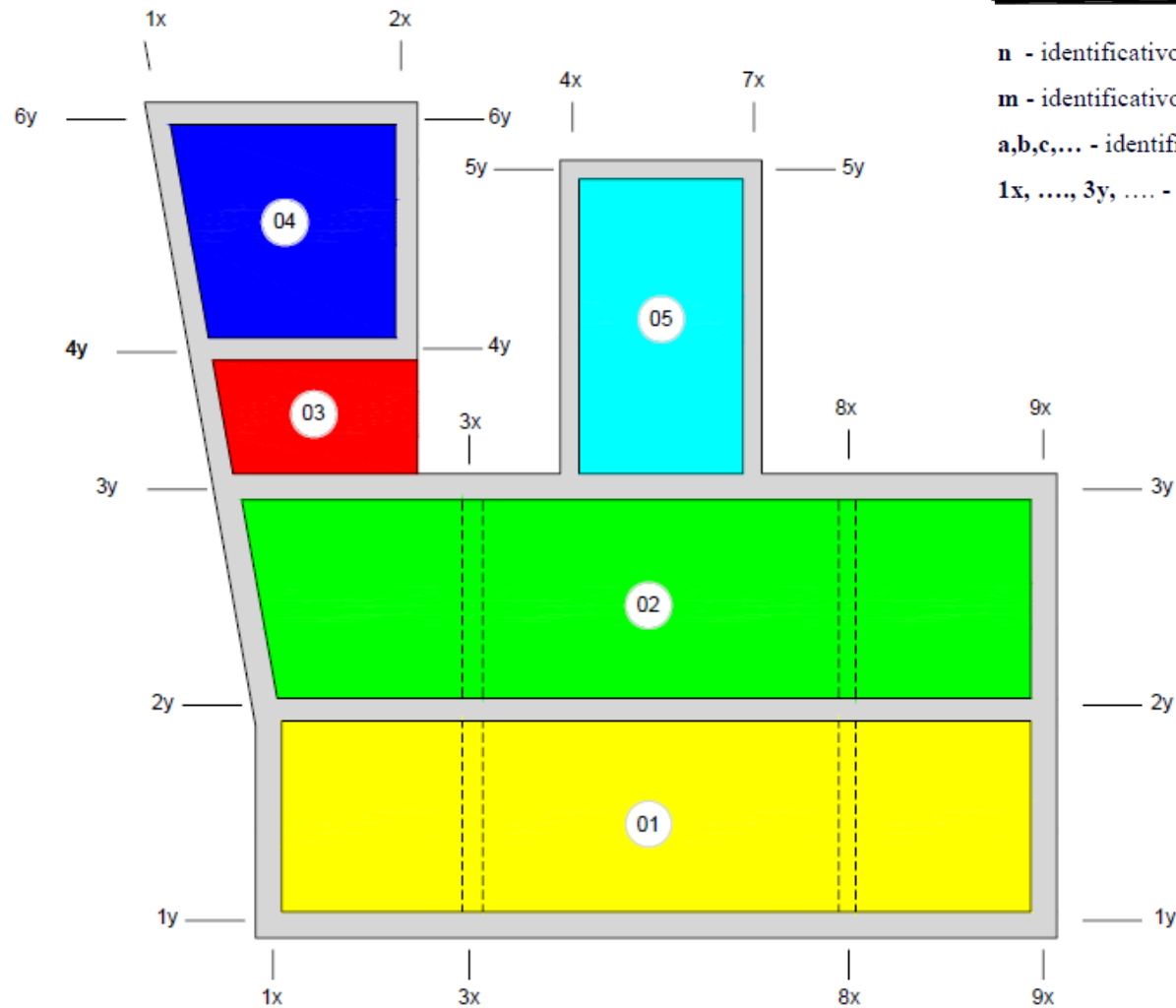


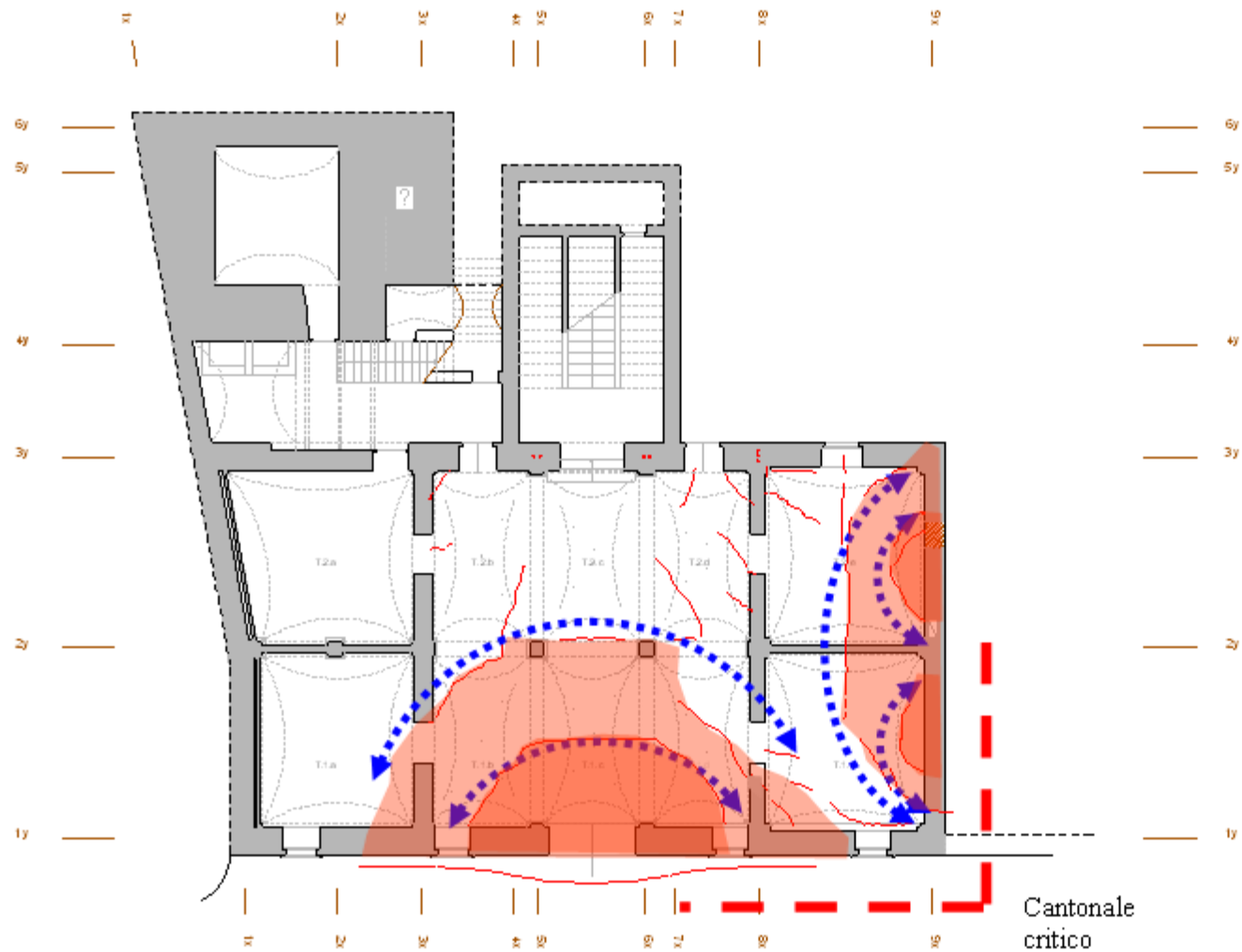
n - identificativo della maglia muraria

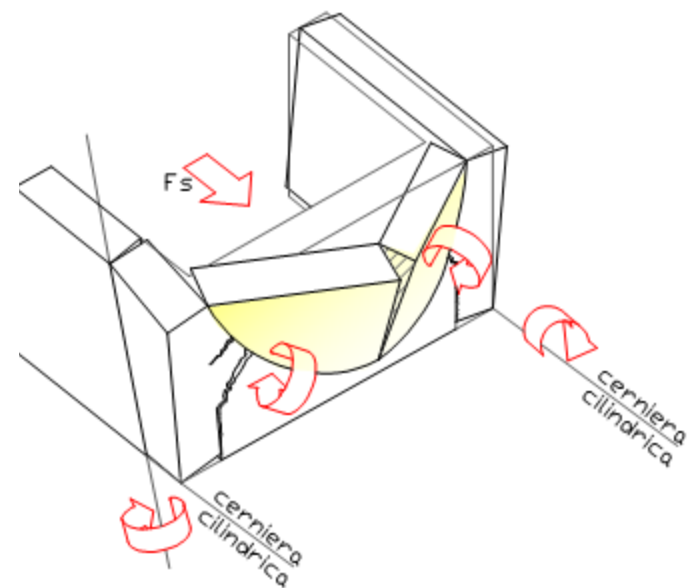
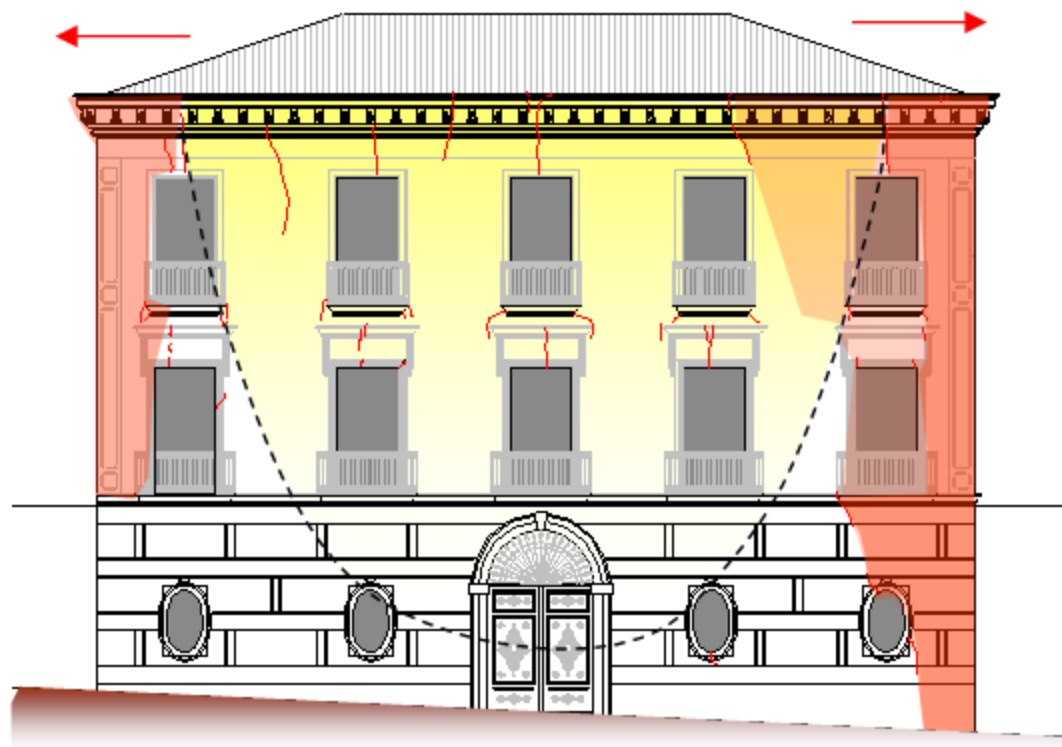
m - identificativo del piano (T, 1, 2, 3)

a,b,c,... - identificativo ambiente

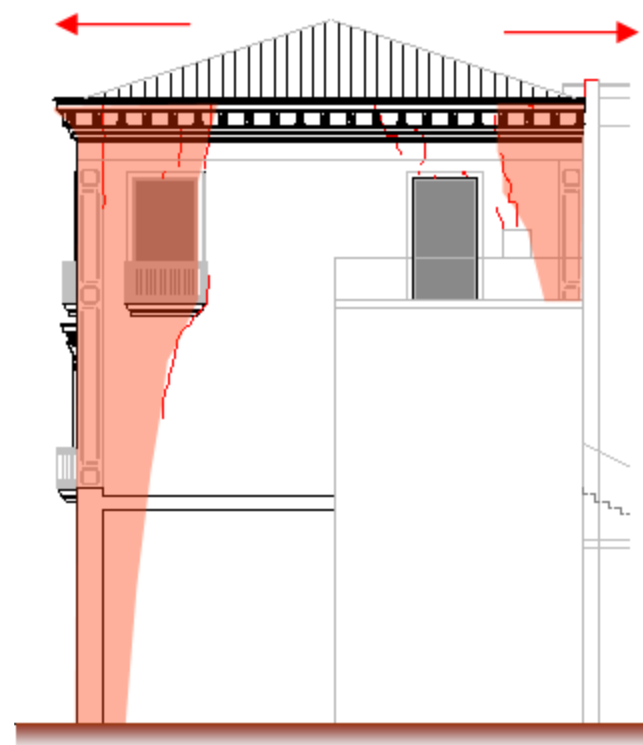
1x, ..., 3y, ... - identificazione delle pareti portanti



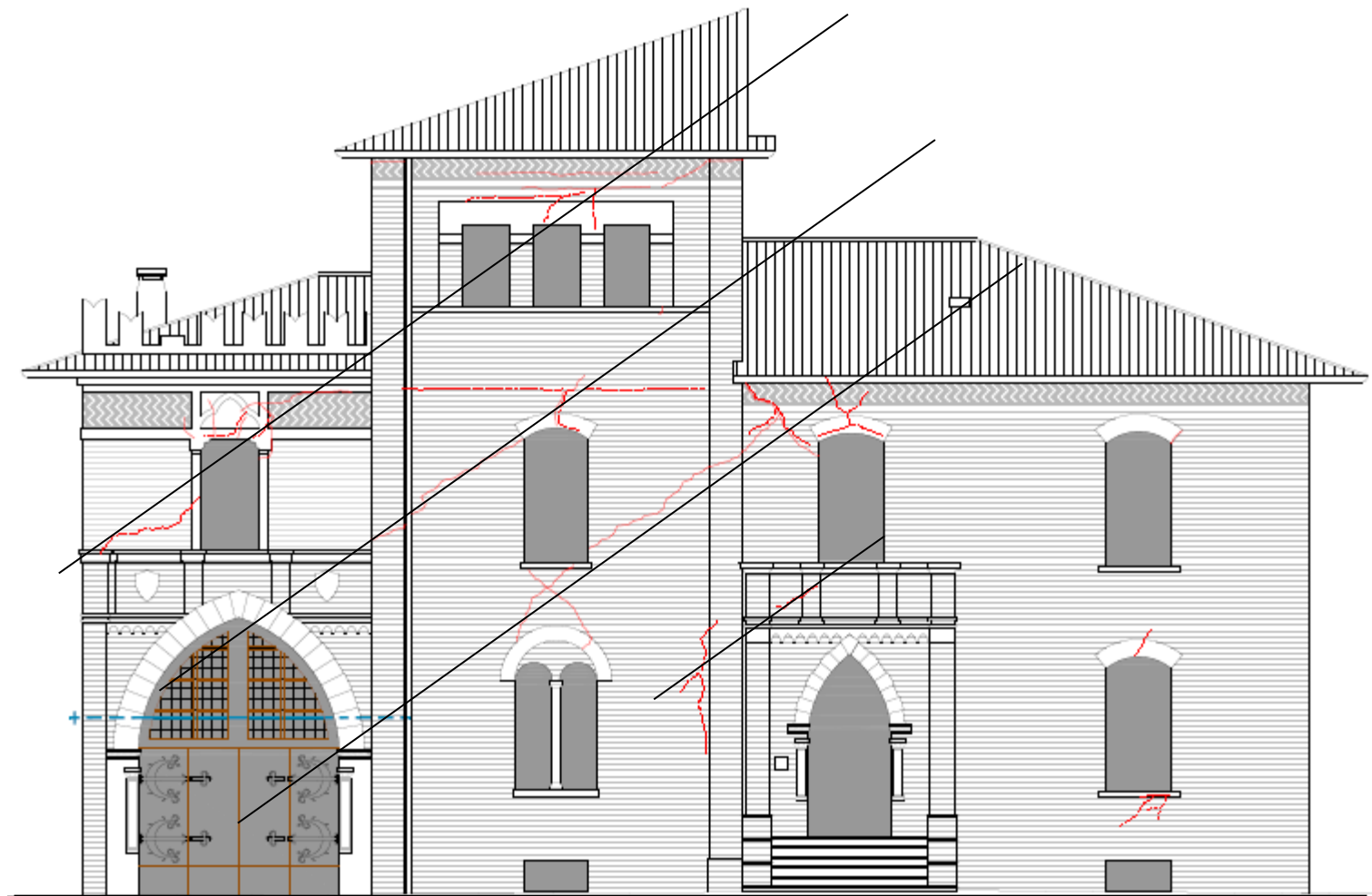
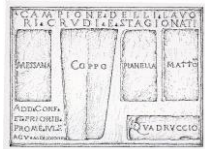


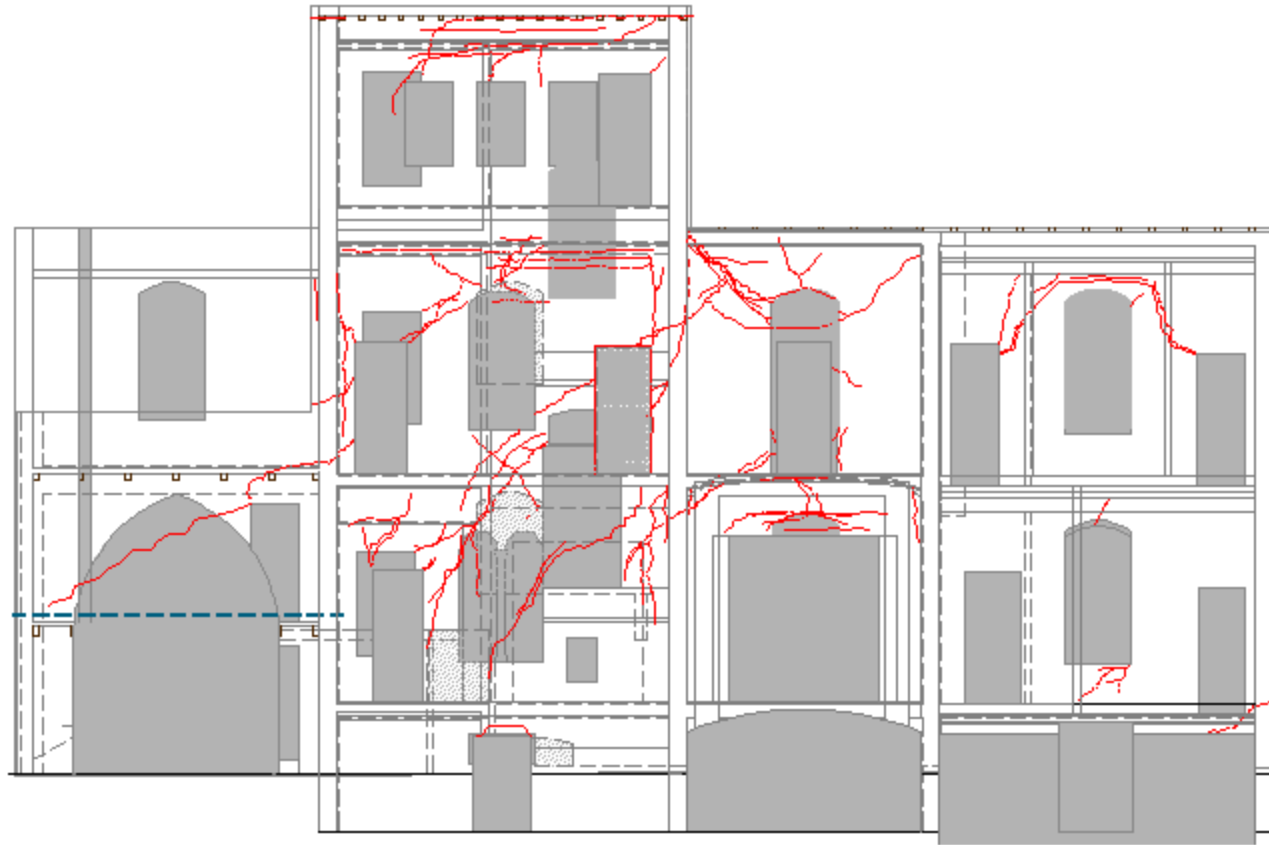


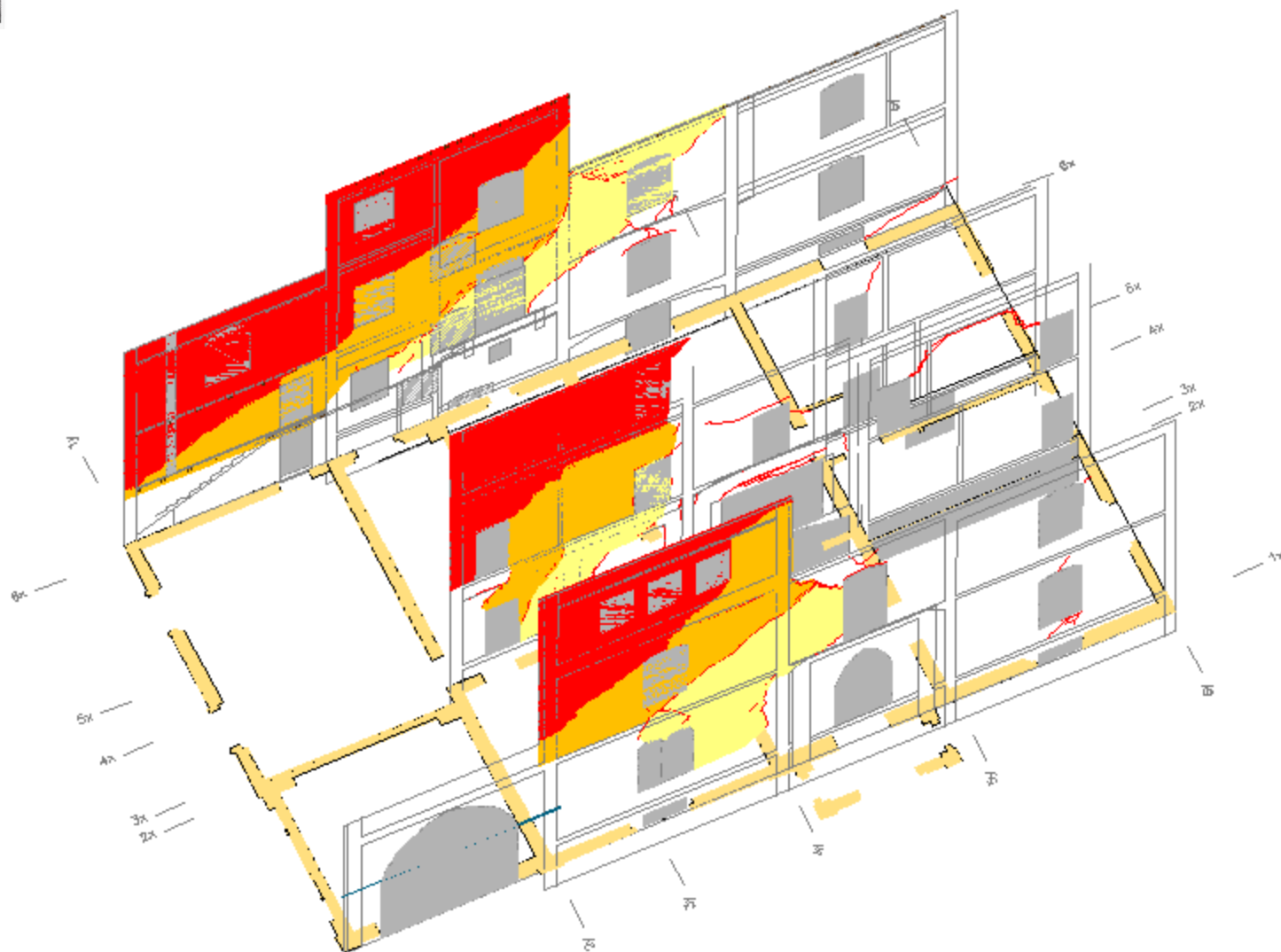
Schema di dissesto della parete di facciata per effetto di azioni sismiche complanari e ortogonali

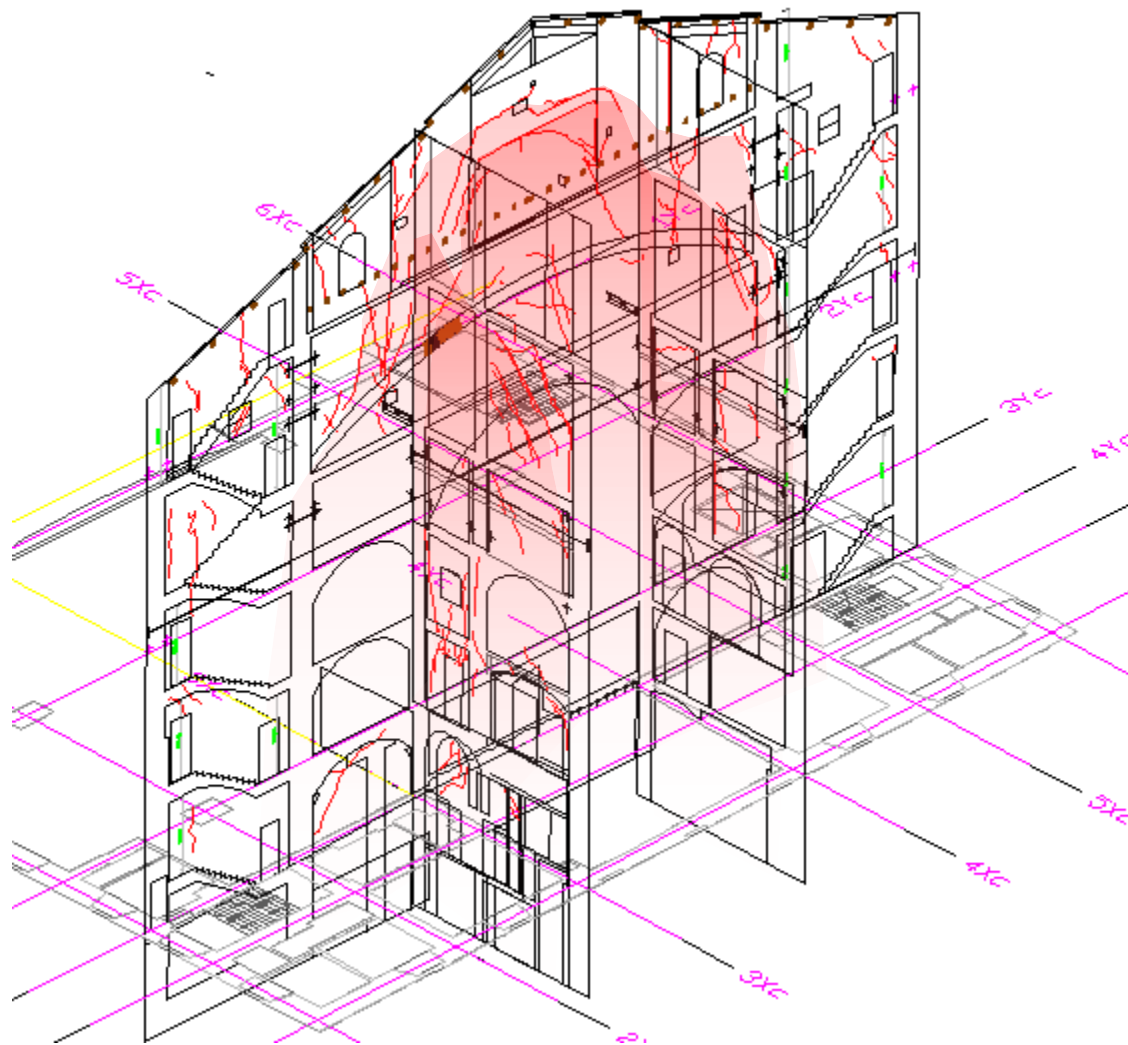


Schema di dissesto della parete laterale di valle per azioni complanari, con dettaglio del quadro fessurativo sommitale d'angolo

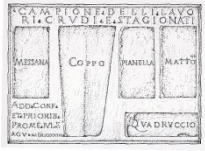




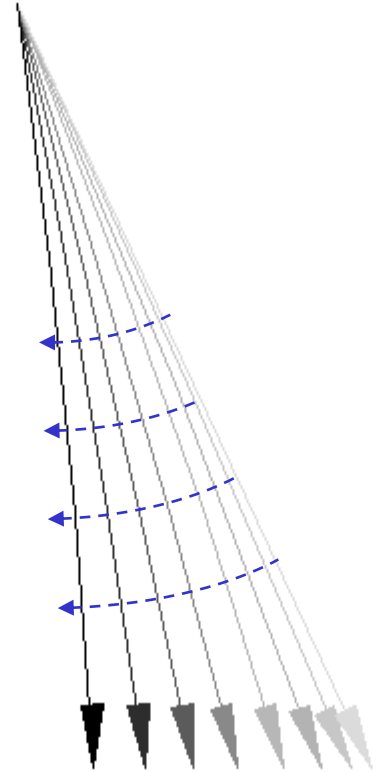
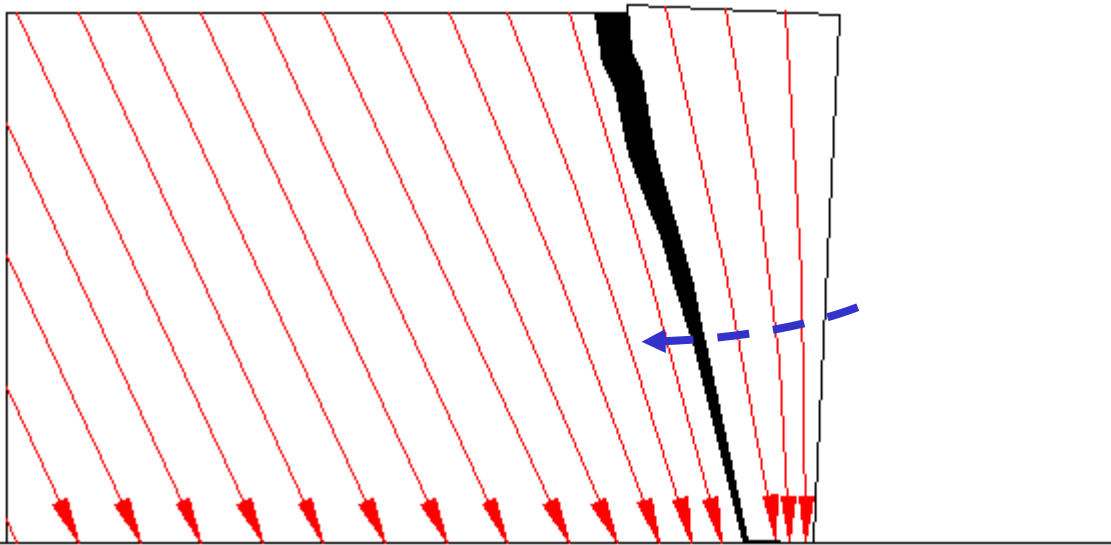
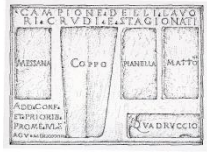


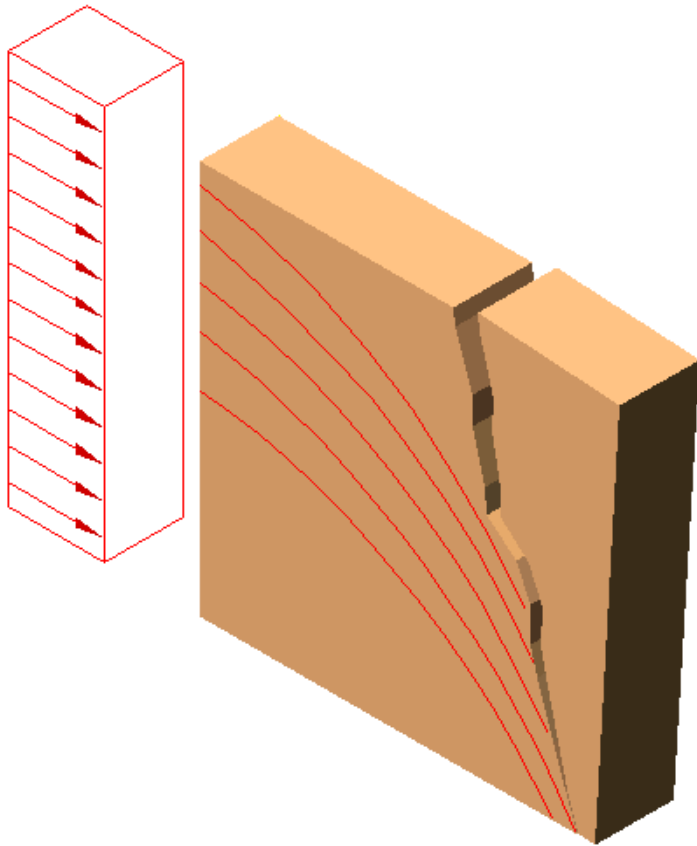
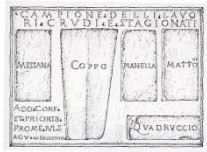


Rappresentazione spaziale di un quadro
fessurativo con manifestazione di
cedimento fondale

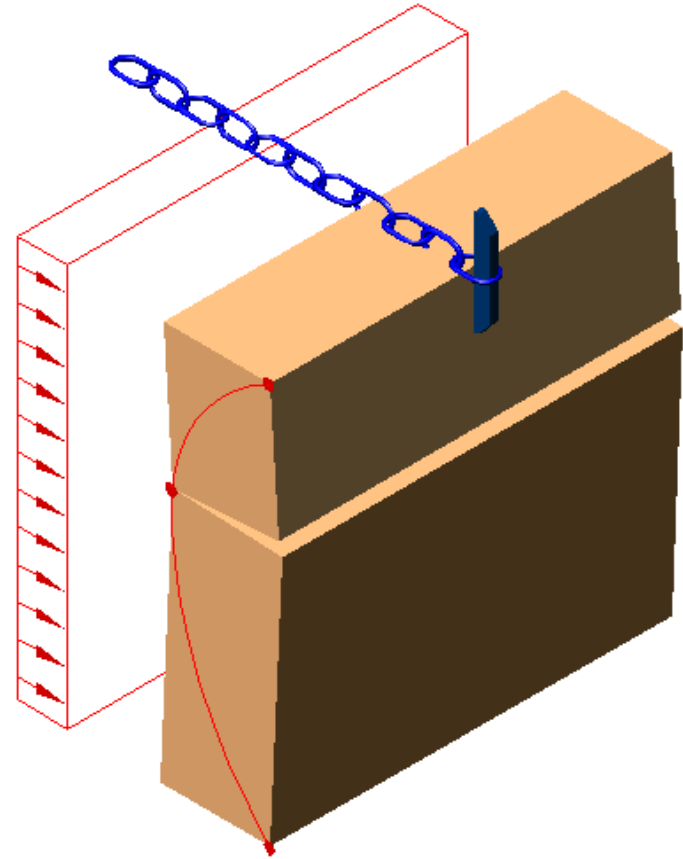
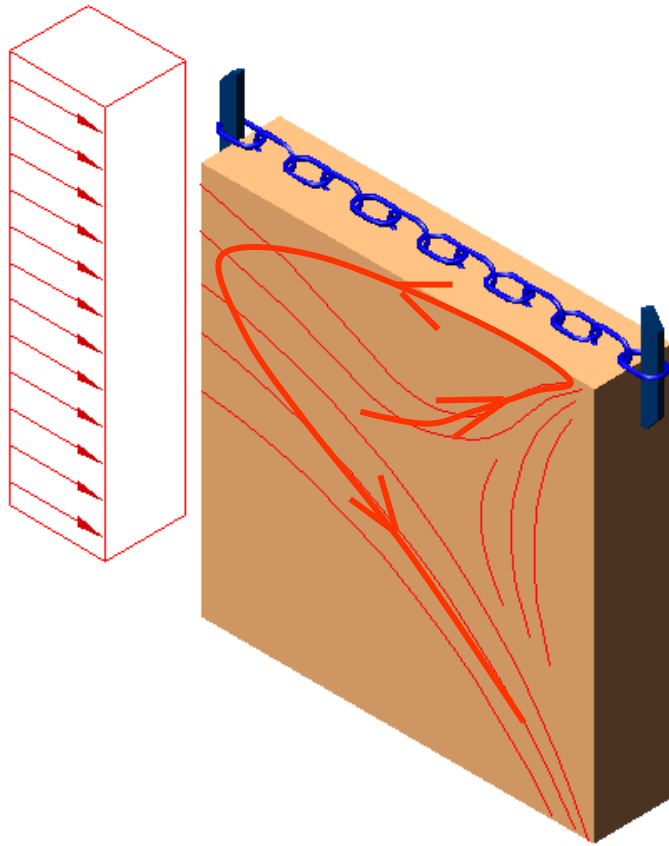
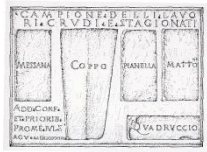


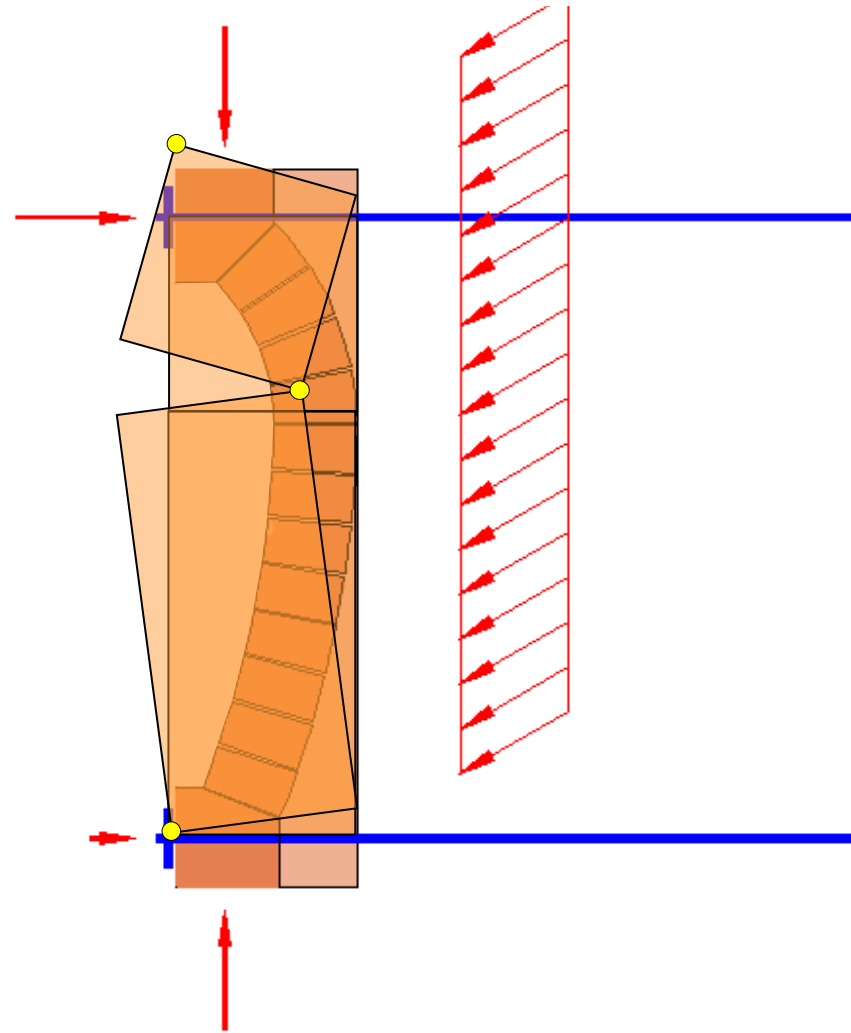
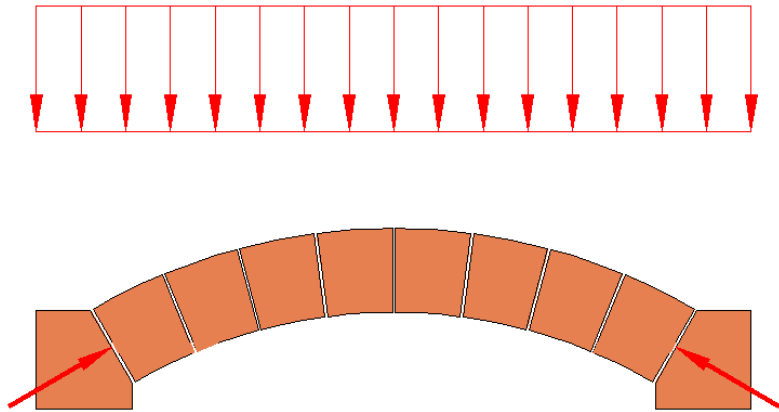
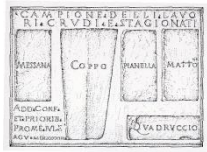
Cinematismi elementari

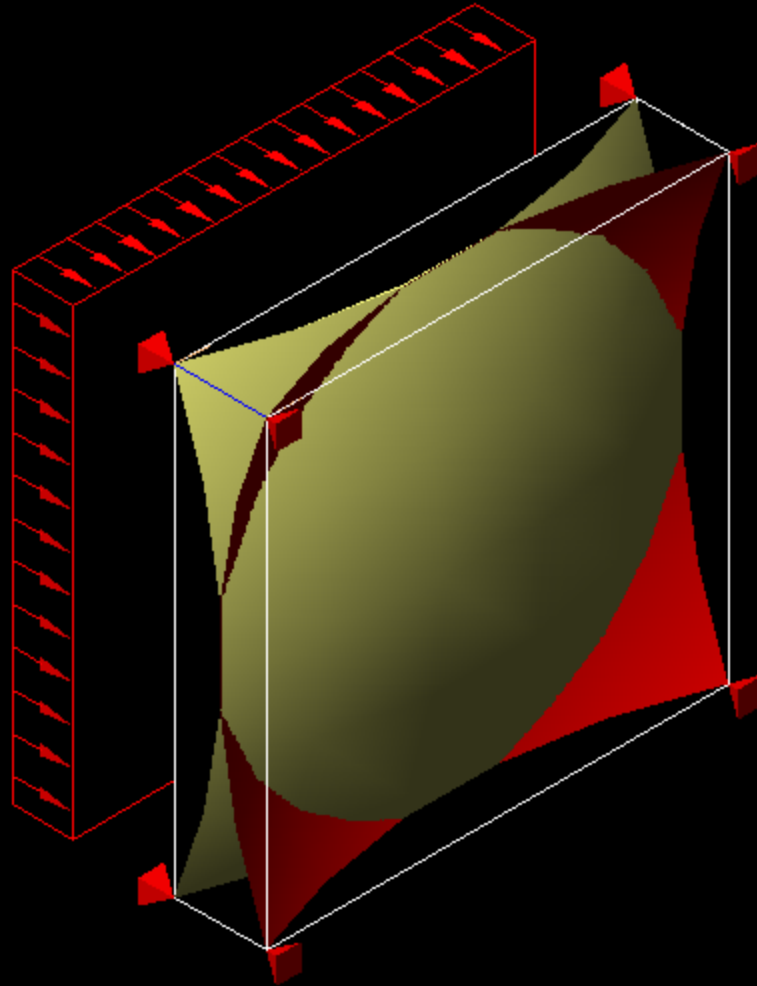


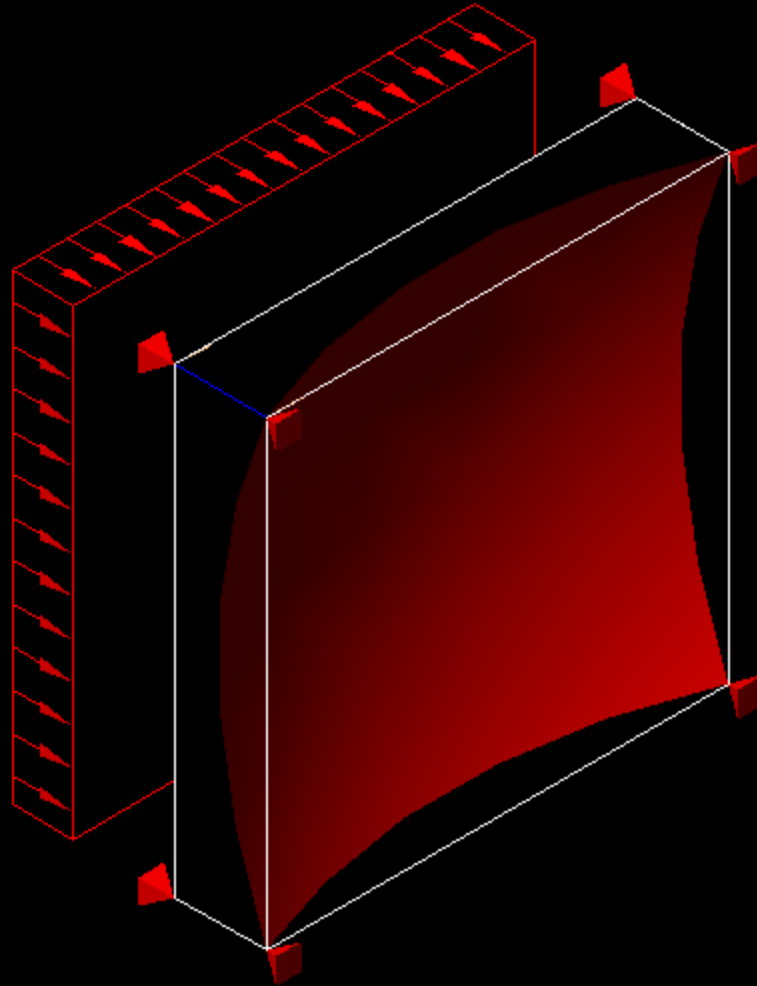


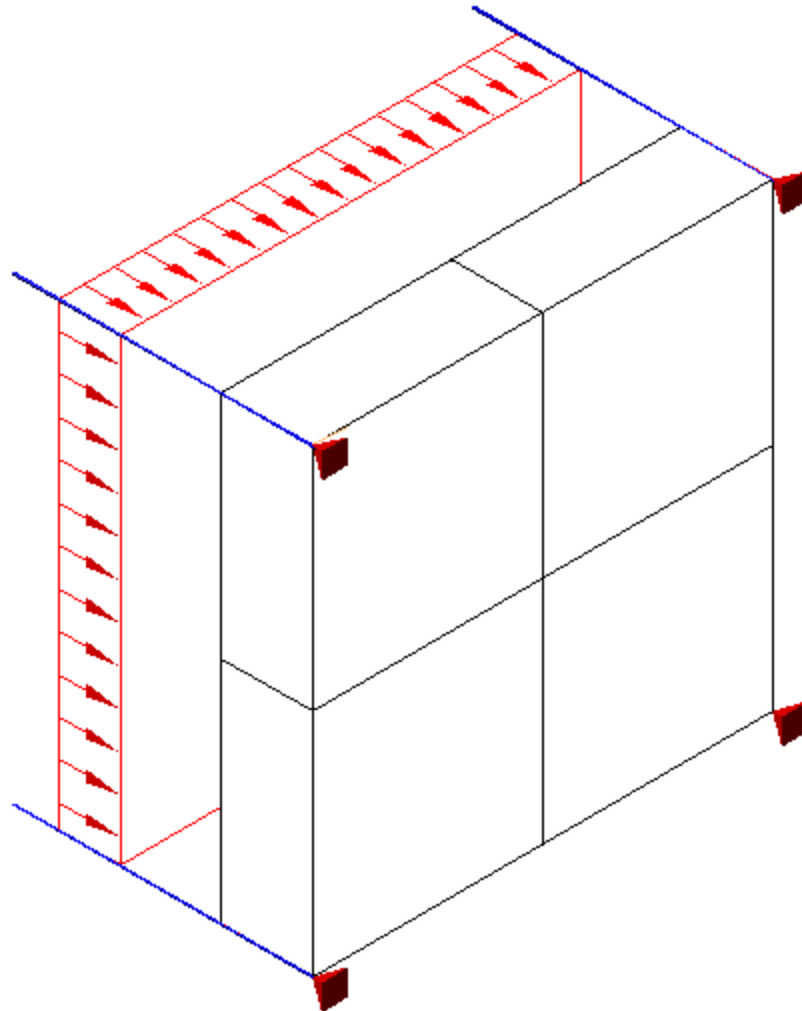
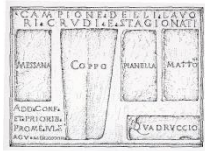


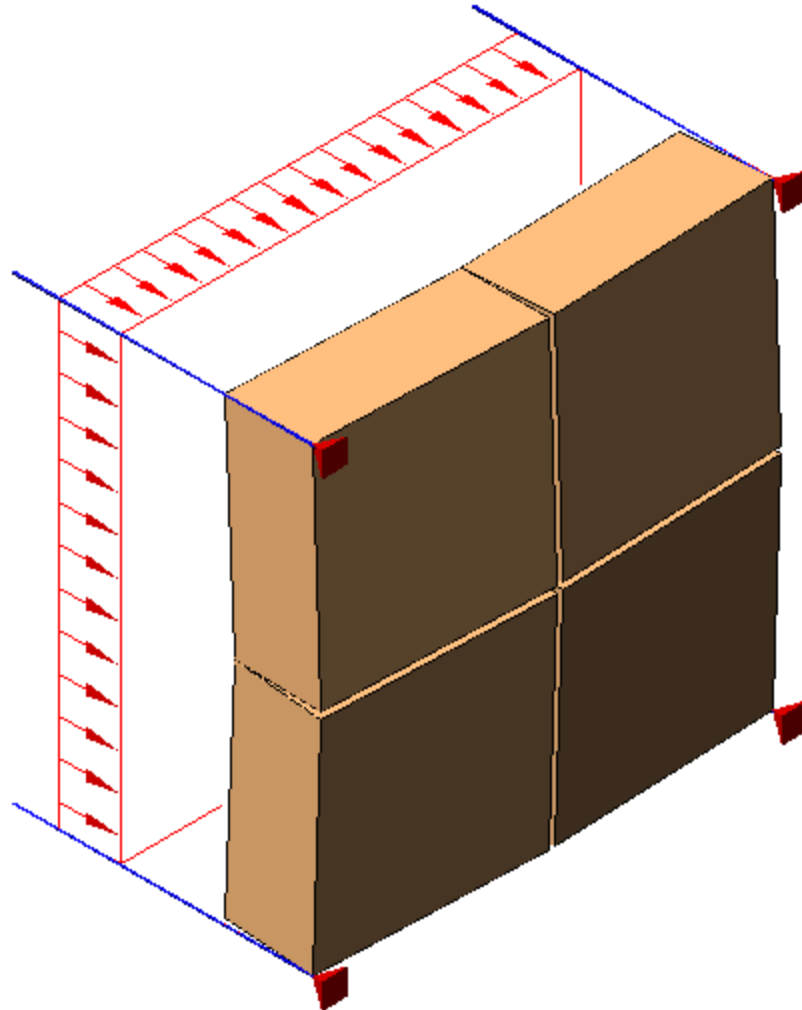
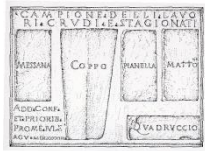


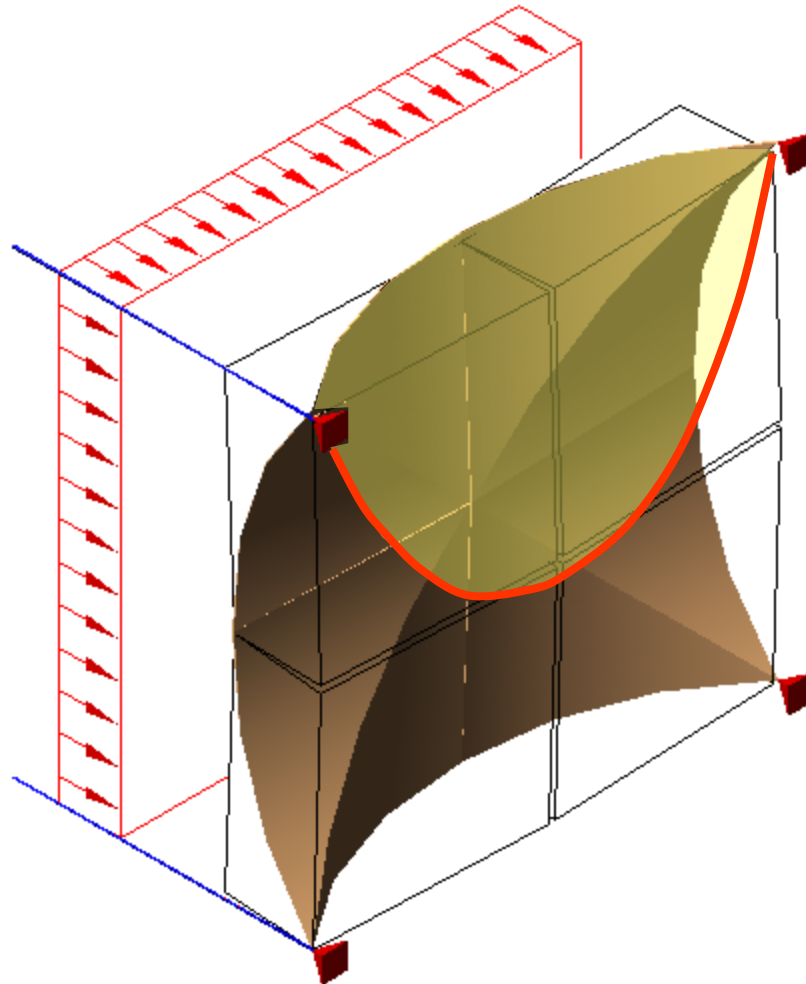
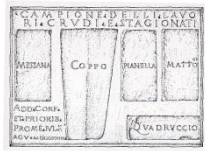


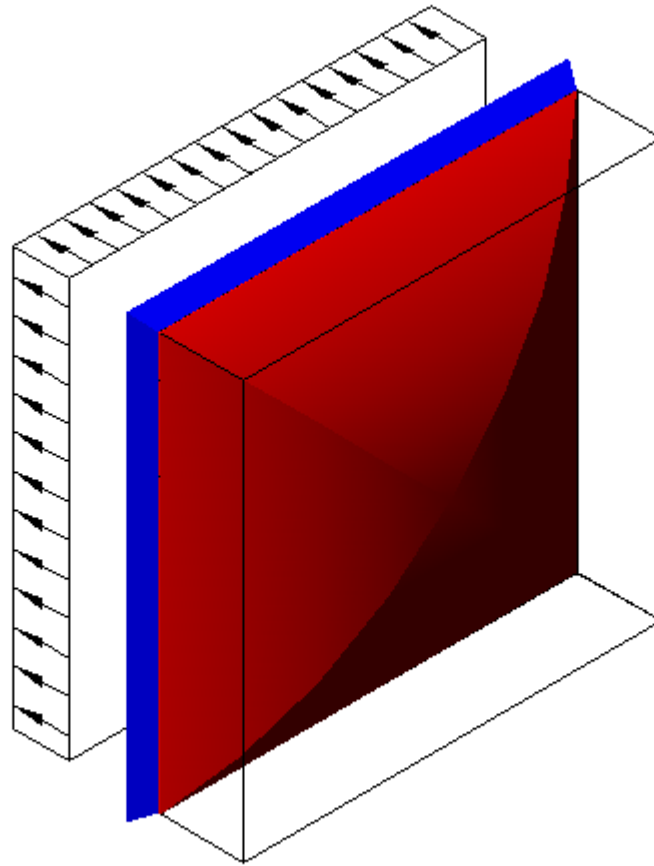
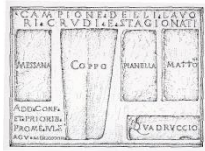


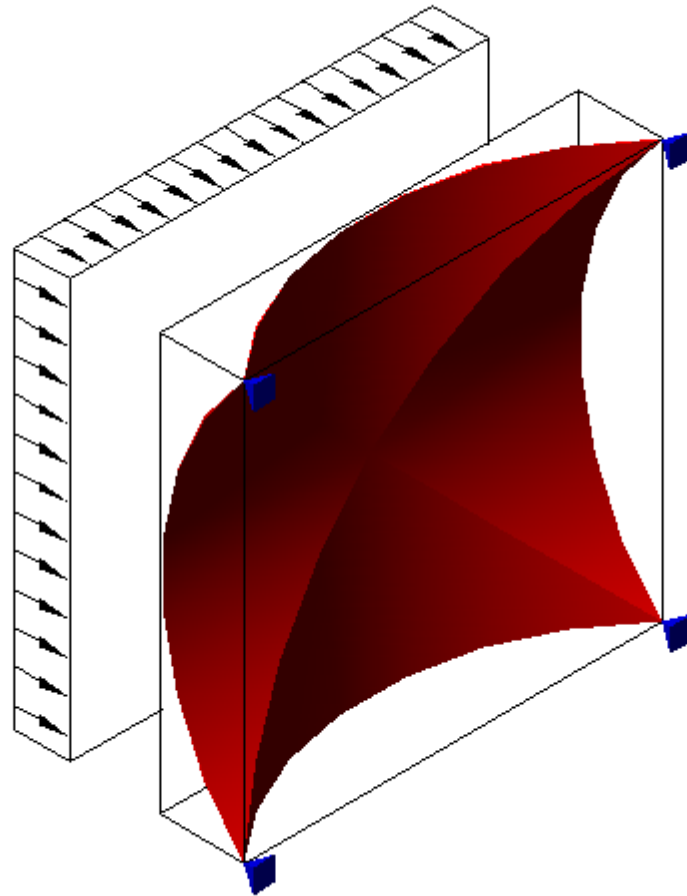
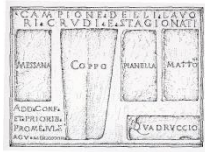


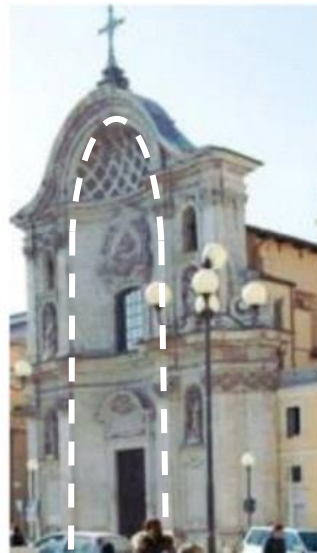
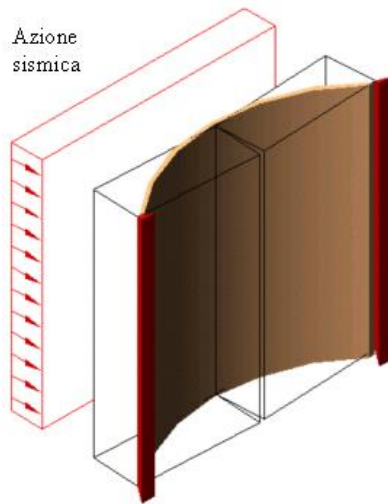




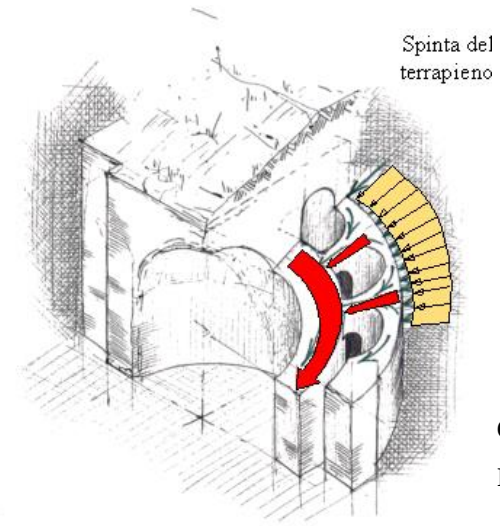




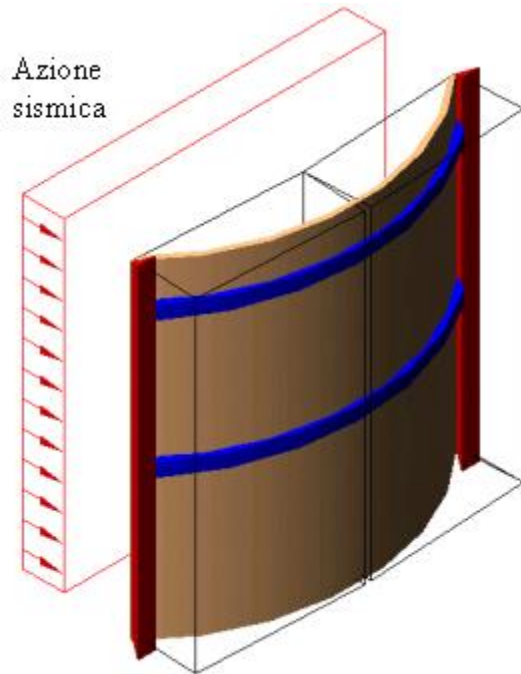




L'Aquila - Chiesa delle Anime Sante

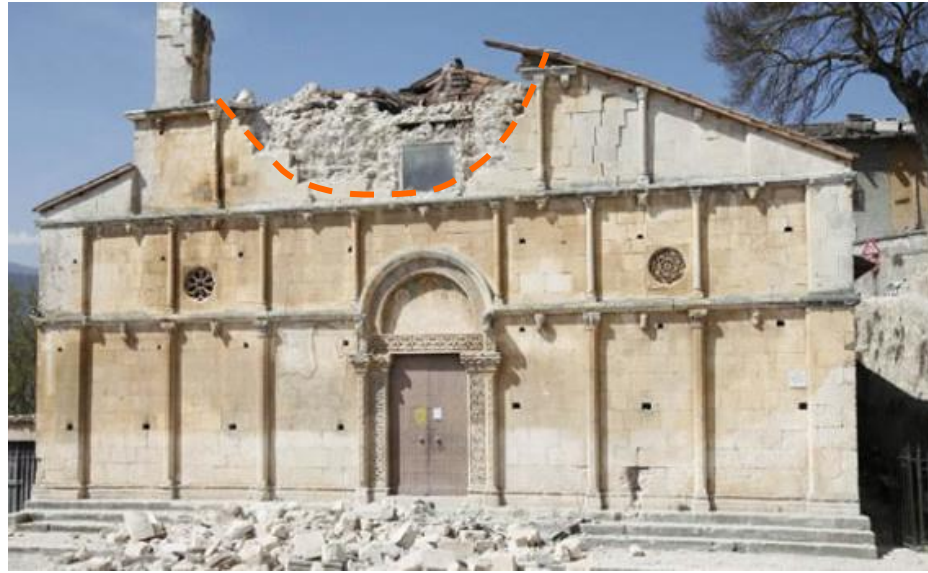
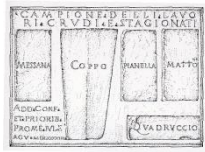


Roma – Podio
del Tempio di
Claudio al Celio
Nicchioni lungo
Via Claudia

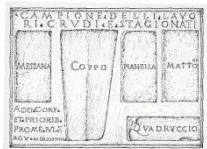


Chiesa dell'Immacolata a Paganica









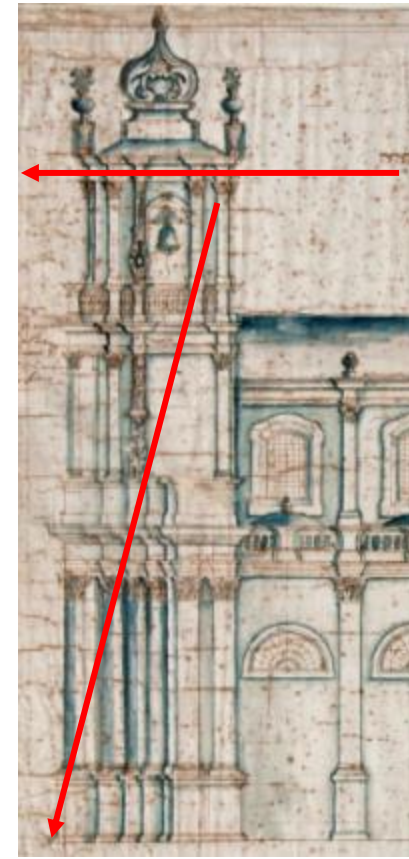
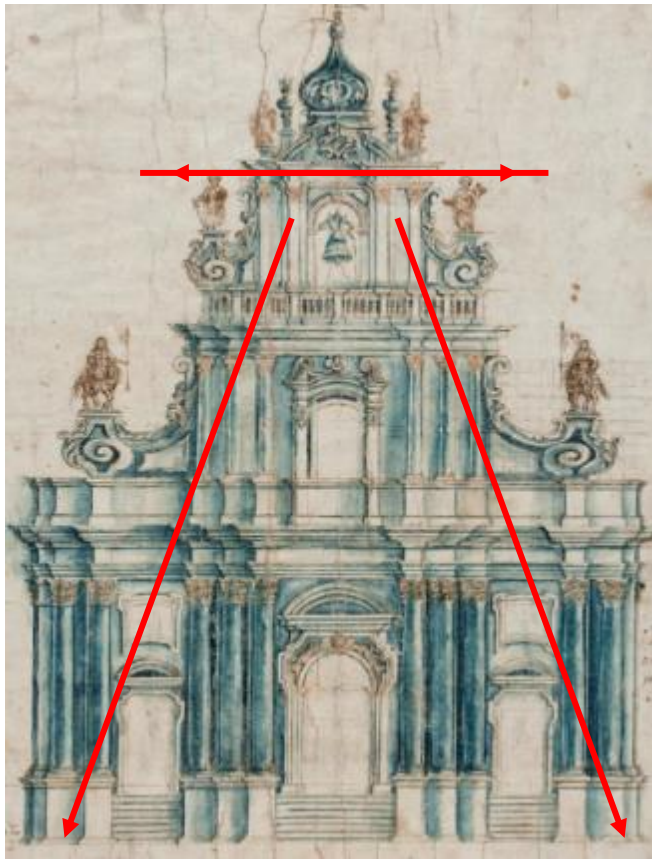
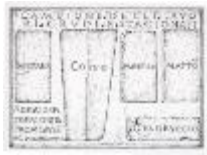
Trarre esperienza dall'osservazione: un esempio indicativo



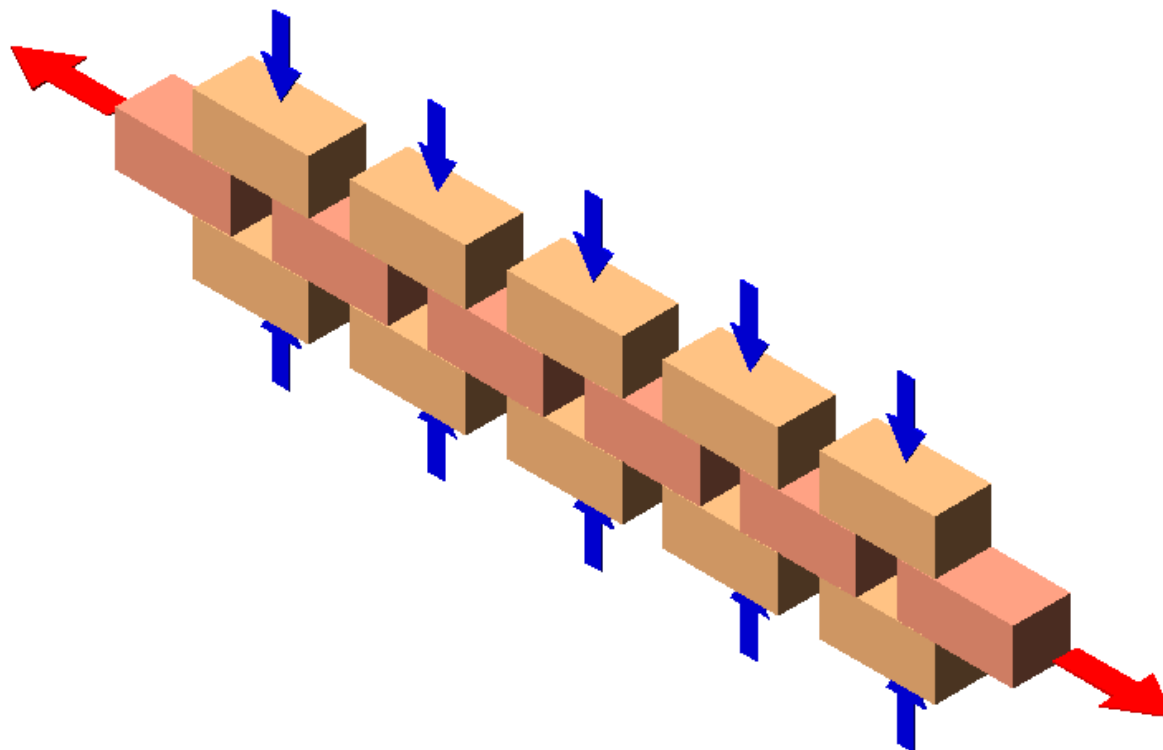
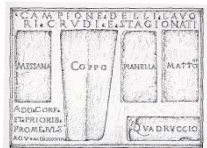
Architettura barocca Siciliana (Scicli)



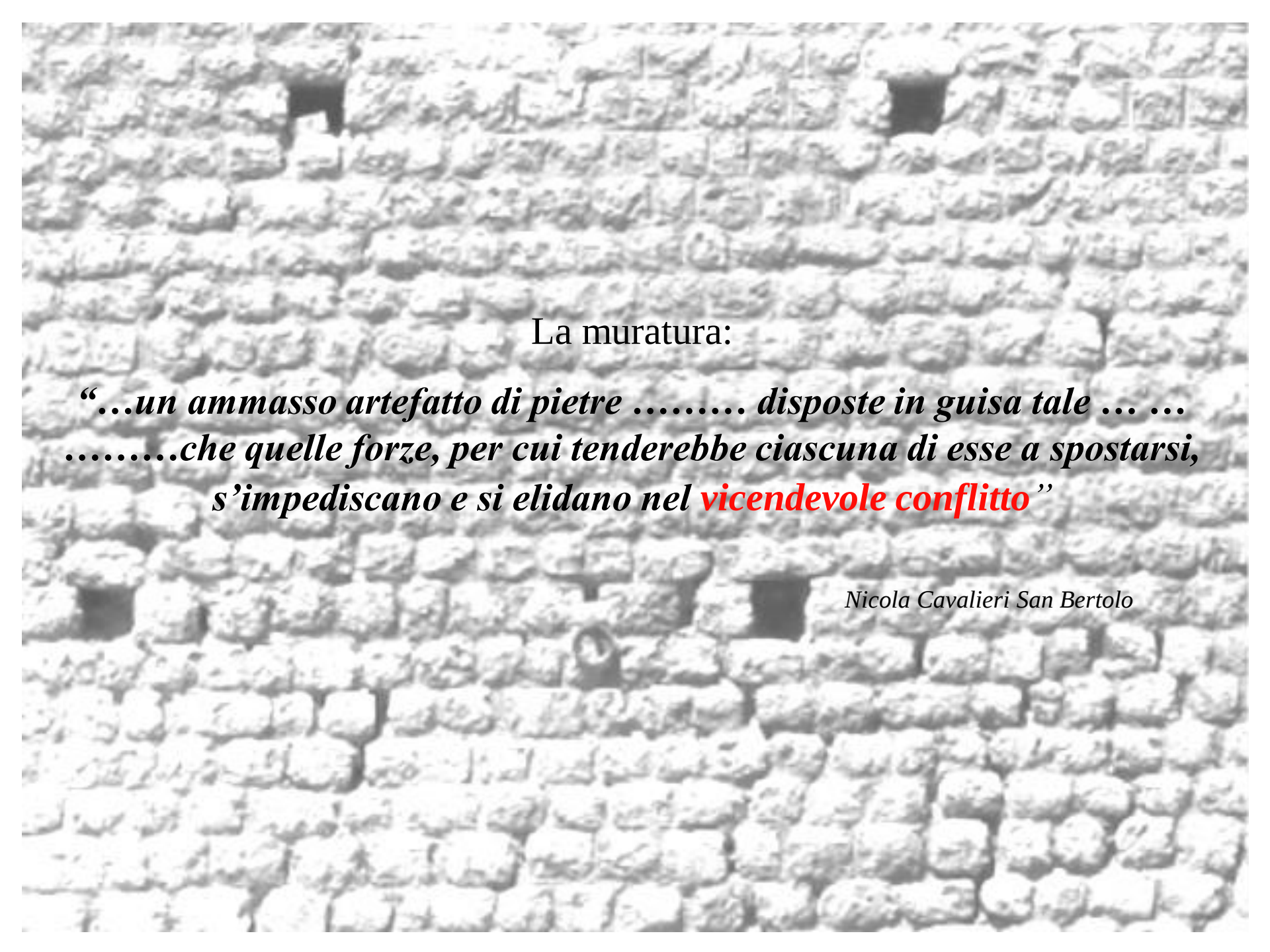
Chiesa paleocristiana presso le Terme di Vespasiano a Cotilia (Rieti)



Architettura barocca Siciliana
(Ragusa – Ibla, Chiesa di San Giorgio, 1744)



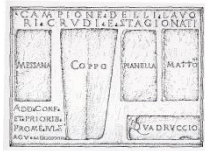
Effetto catena nelle murature incatenate, garantito
dall'attrito sulle superfici di contatto fra gli
elementi e dalla coesione della malta



La muratura:

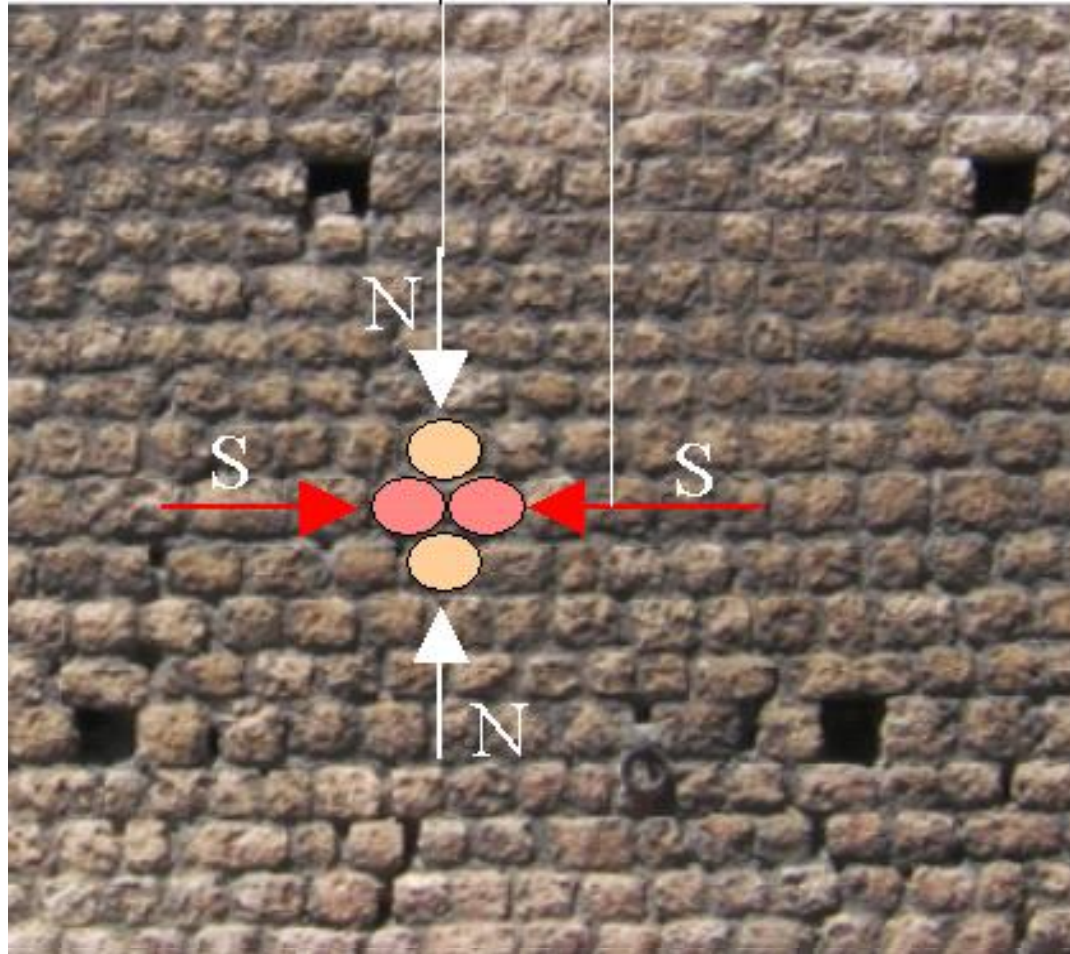
*“...un ammasso artefatto di pietre disposte in guisa tale
.....che quelle forze, per cui tenderebbe ciascuna di esse a spostarsi,
s’impediscano e si elidano nel **vicendevole conflitto**”*

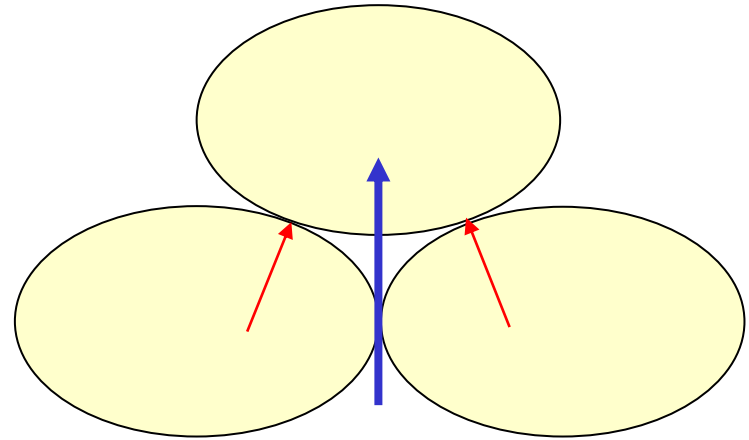
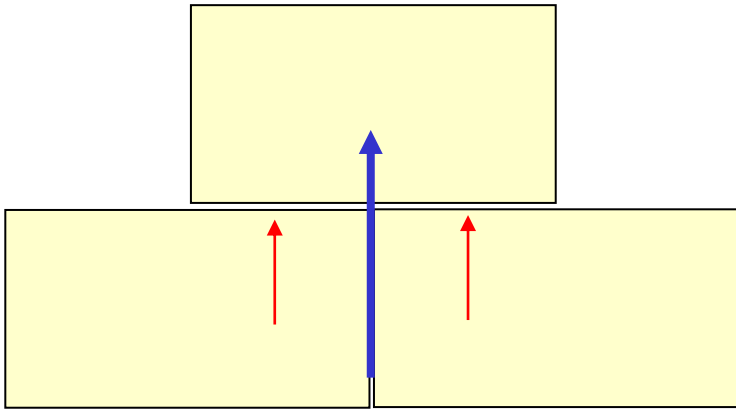
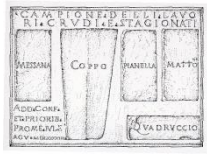
Nicola Cavalieri San Bertolo

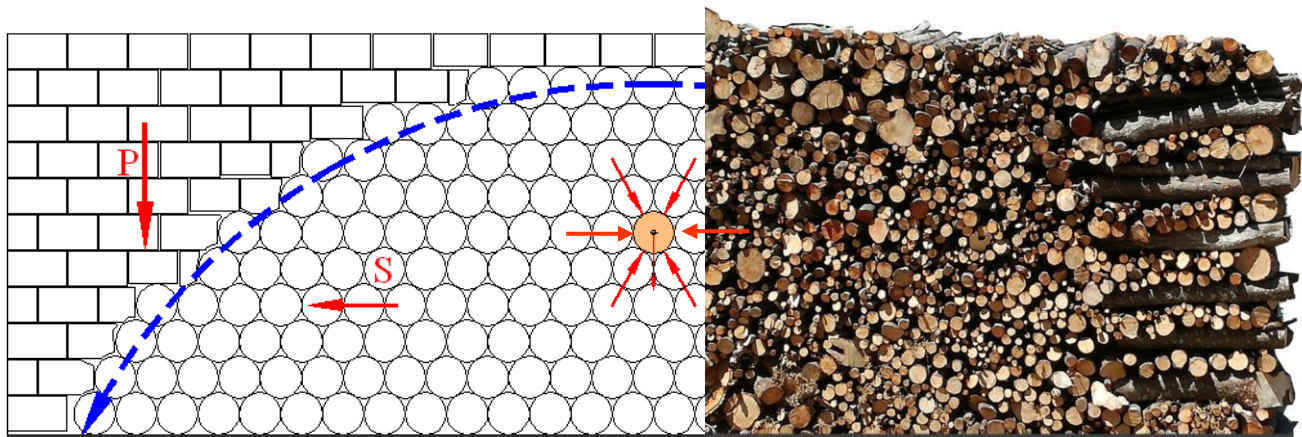


Sforzo di
compressione

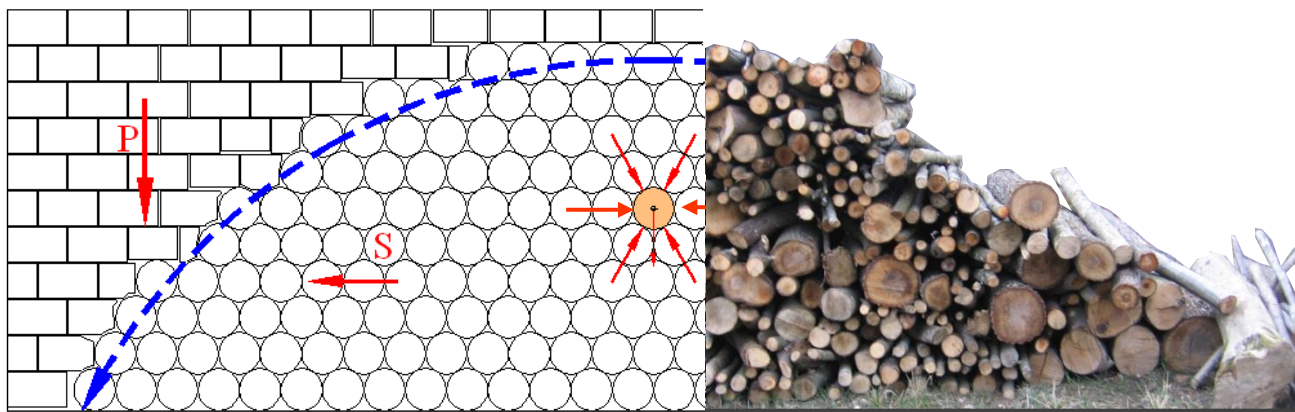
Spinta di
contrasto







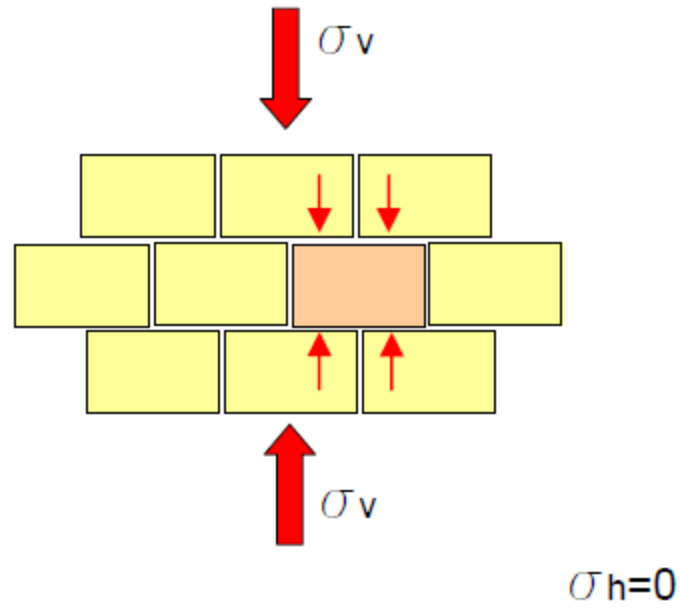
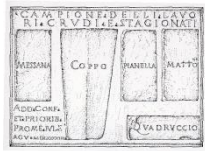
Modello di parete muraria con stato di “precompressione orizzontale” e testate di contrasto in blocchi squadrati

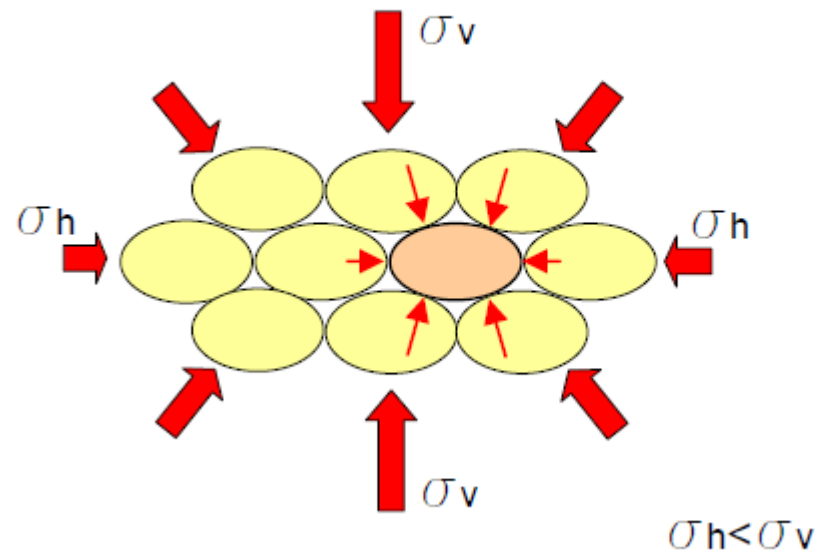
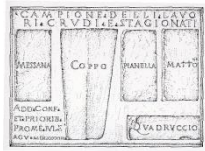


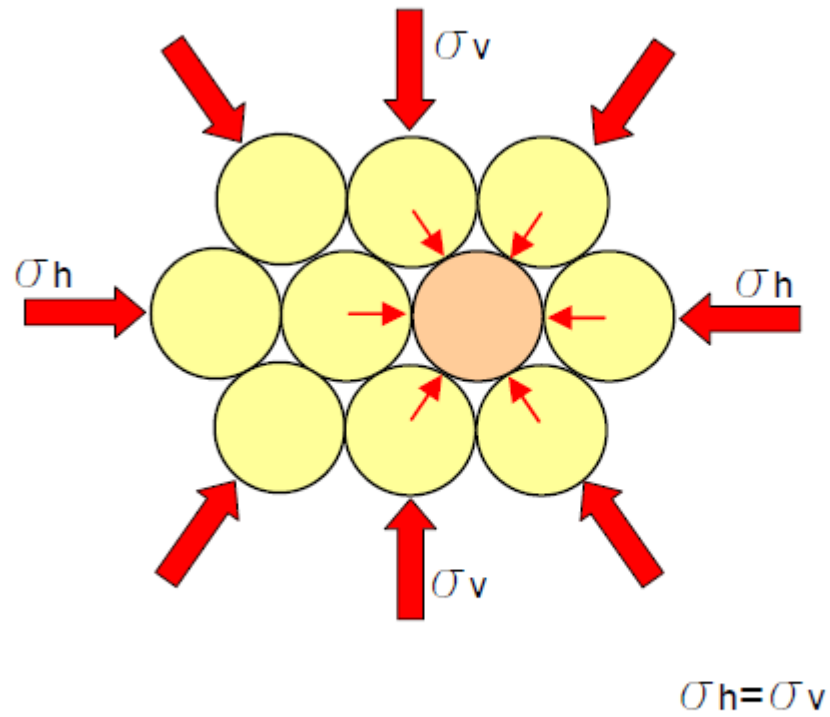
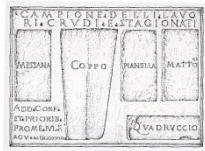
Modello di parete muraria con stato di “precompressione orizzontale” e testate di contrasto in blocchi squadretti

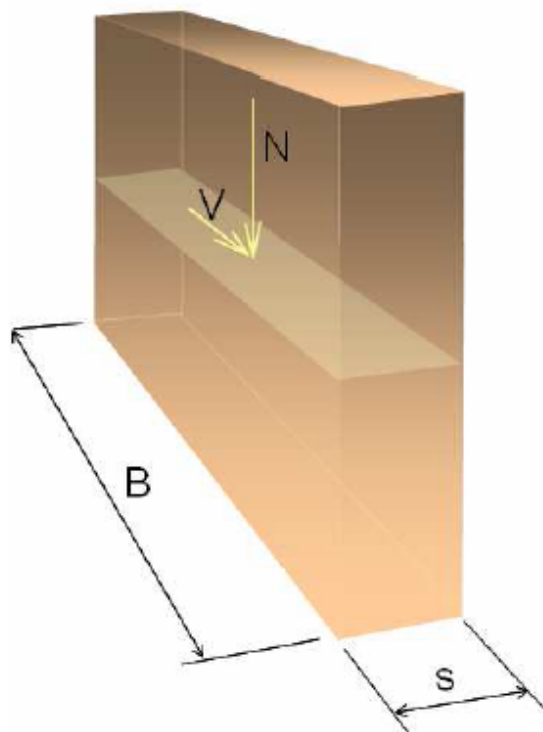
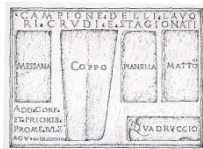


Palmira (Siria) – Rovine del tempio di Bel, con paramento costituito da rocchi di colonne riusate.
Foto: F.Giovanetti









Caratteristiche geometriche:

s=	0,40 ml
B=	1,80 ml
<i>Sollecitazioni:</i>	
N=	30000 daN
$\sigma_v =$	4,17 daN/cm ²
$\alpha = \sigma_h / \sigma_v =$	0,20
$\sigma_h =$	0,83 daN/cm ²
<i>Resistenza a taglio:</i>	
$\tau_o =$	0,40 daN/cm ²

α	τ_u (daN/cm ²)	rapporto +	Taglio ultimo $V_u = B \cdot s \cdot \tau_u$	
0	1,13	1,00	8.118	daN
0,1	1,47	1,30	10.567	daN
0,2	1,74	1,55	12.546	daN
0,3	1,98	1,76	14.254	daN
0,4	2,19	1,94	15.778	daN
0,5	2,38	2,11	17.167	daN
0,6	2,56	2,27	18.451	daN
0,7	2,73	2,42	19.652	daN
0,8	2,89	2,56	20.784	daN
0,9	3,04	2,69	21.857	daN
1	3,18	2,82	22.880	daN

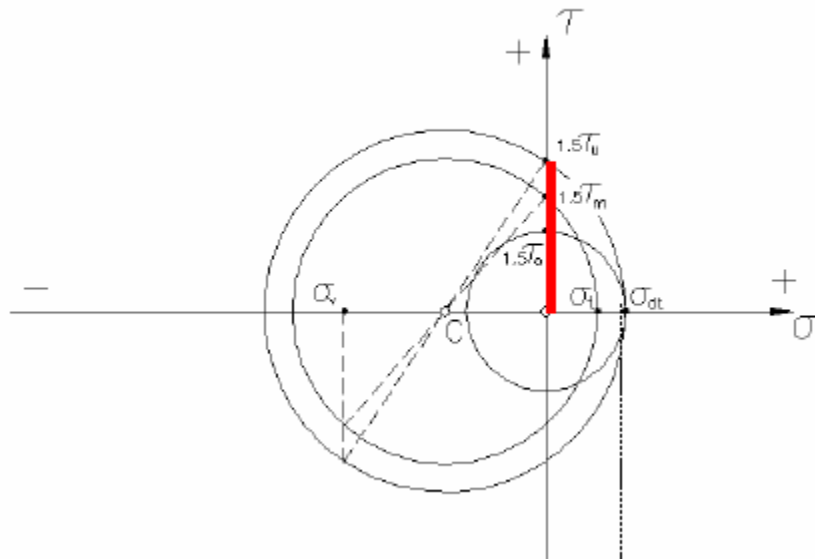
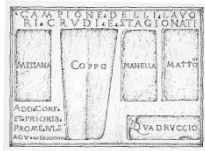
$$\tau_u = \tau_o \sqrt{1 + \frac{\sigma_v}{1,5 \tau_o}}$$

se $\alpha=0$ Formula di Turnsek - Cacovic

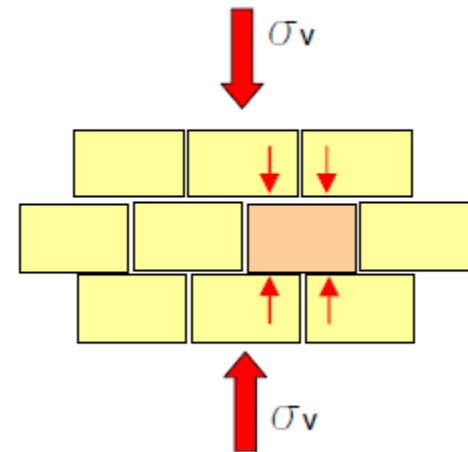
$$= 1,13 \text{ daN/cm}^2$$

$$\tau_u = 2/3 \cdot \sqrt{[(\sigma_v + \sigma_h)/2 + 1,5 \tau_o]^2 - ((\sigma_v - \sigma_h)/2)^2}$$

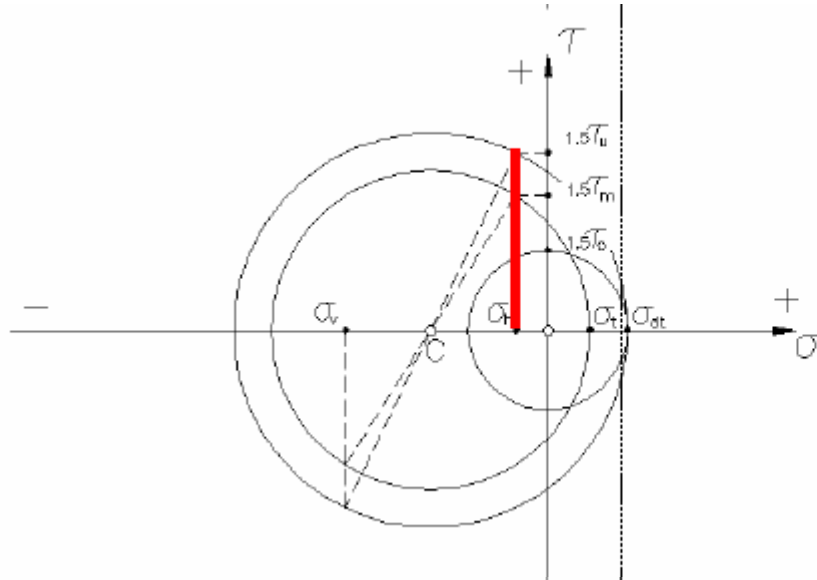
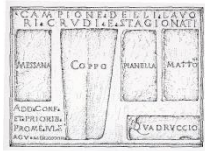
$$= 1,74 \text{ daN/cm}^2$$



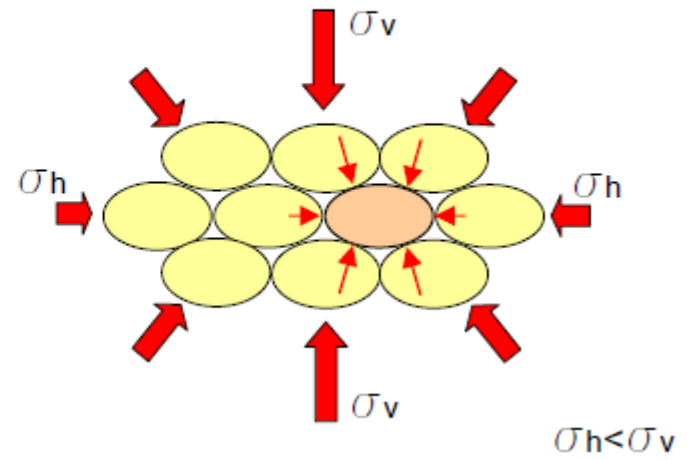
A)

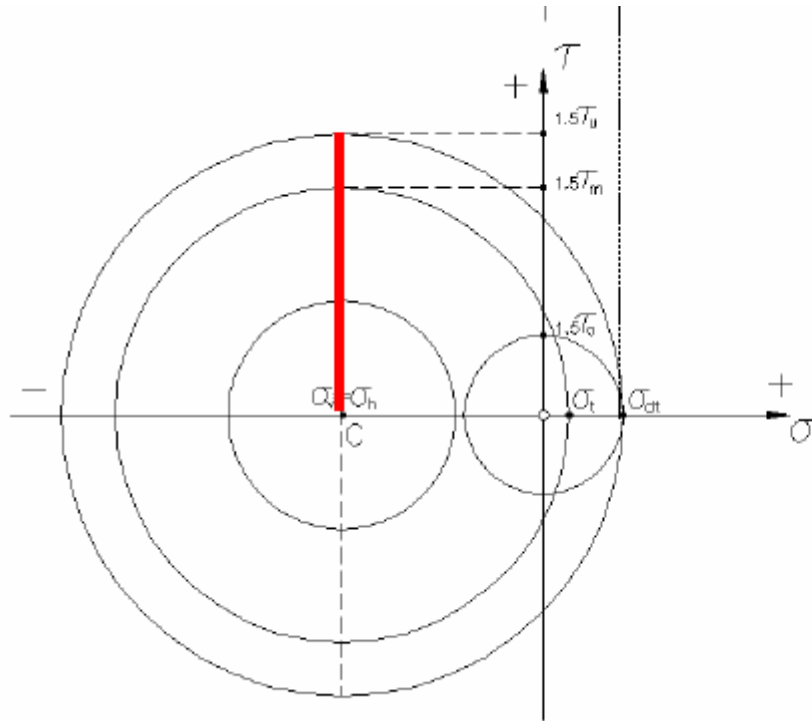
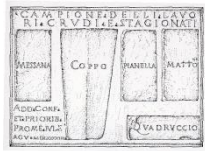


$$\sigma_h=0$$

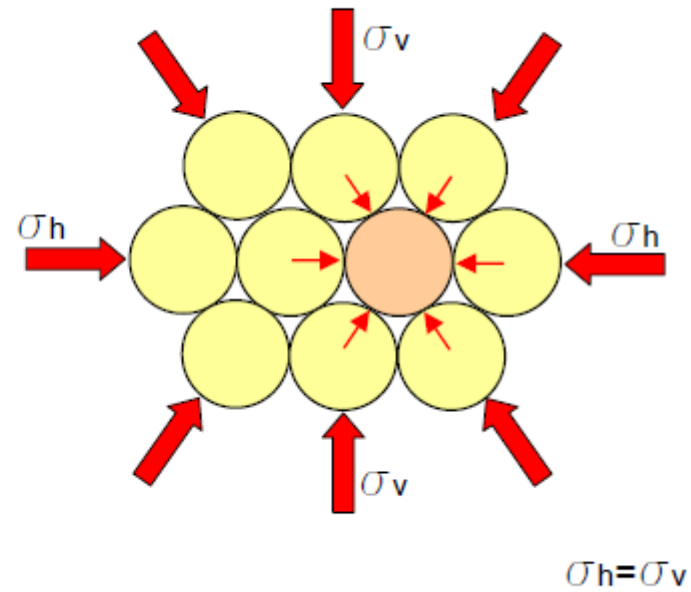


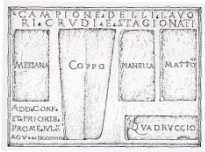
B)





c)





Caratterizzazione meccanica dei materiali

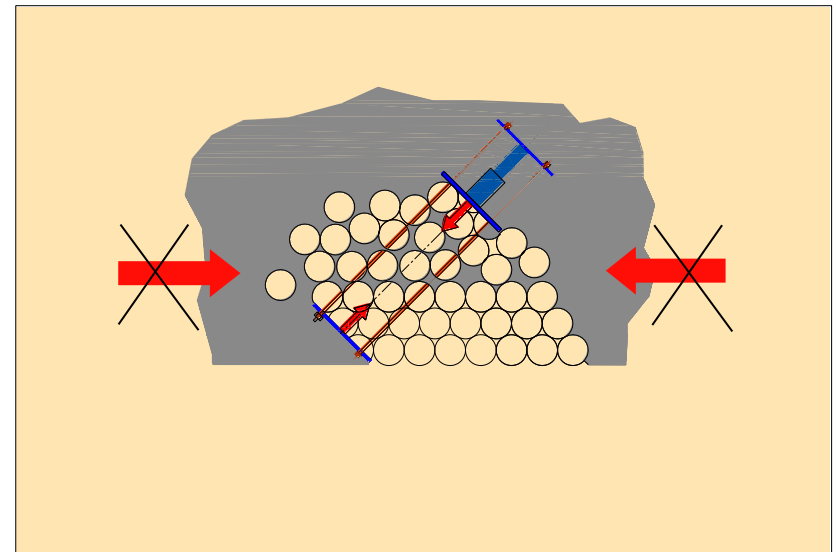
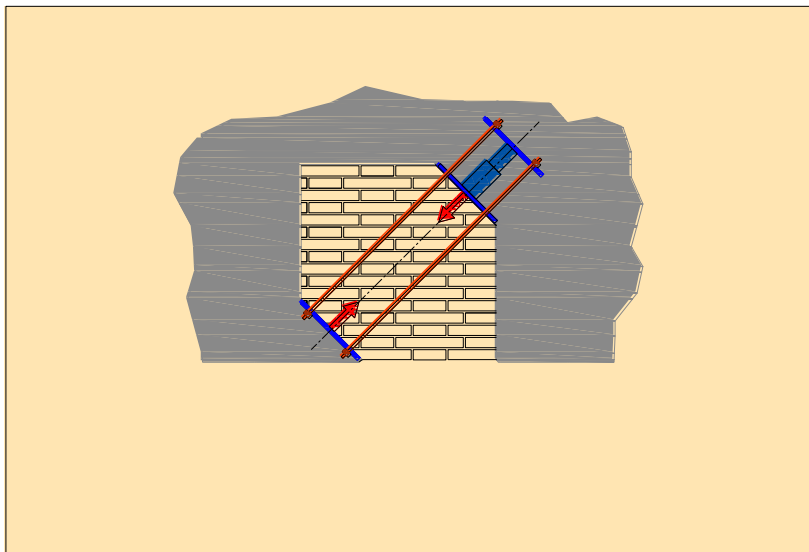
- Valutazione delle caratteristiche meccaniche e livello di degrado dei materiali tramite:

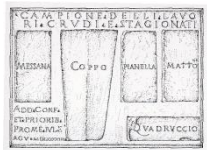
- . verifiche visive in situ
- . analisi dati già disponibili
- . prove sperimentali

Livelli di conoscenza

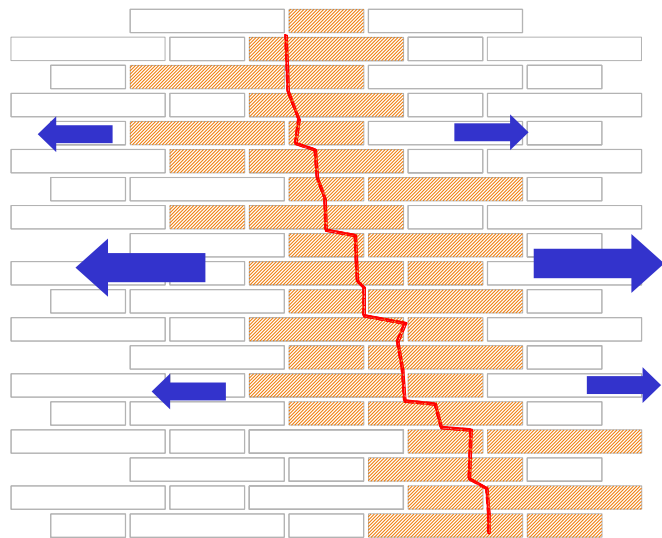
(LC1, LC2 e LC3)

Indagini limitate, estese, esaustive

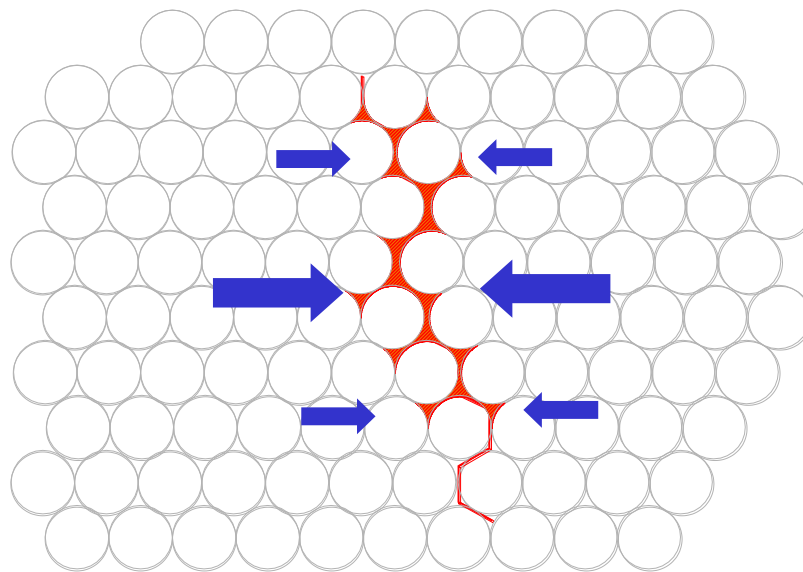




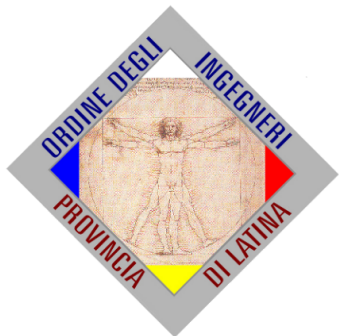
Interventi di cucì-scucì



Ripristino dell'ingranamento e della resistenza a trazione equivalente per attrito e coesione



Ripristino dell'azione di contrasto e dello stato di precompressione



ORDINE DEGLI INGEGNERI DELLA PROVINCIA DI LATINA

con il contributo incondizionato di



Seminario webinar "RINFORZO E CONSOLIDAMENTO STATICO E ANTISISMICO DEGLI EDIFICI ESISTENTI"

Principi di meccanica delle murature e di archi e volte per la valutazione del comportamento statico e della risposta sismica degli edifici storici in riferimento al quadro normativo.

Analisi del danno e delle lesioni sugli edifici storici, casistiche e approccio alla lettura del quadro fessurativo

Ing. Giovanni Cangi – libero professionista